PREDEVELOPMENT

Volume 2 of 3 Vol. 1: pages 1-33 Vol. 2: pages 34-136 Vol. 3: pages 137-241

Point of Analysis A







37

Drainage Area Runoff and Time of Concentration

Drainage Area: To 460 northern culvert crossing (excl. Union) PREDEVELOPMENT

| | C | omposite Curve Numl | per (CN) | | | Notes: |
|------------------|-----------------|---------------------|----------|---------------|---------|--------|
| | Hydrologic Soil | | | | | |
| | Group | Land Cover | CN | Area, A (ac.) | CN*A | |
| CN ₁ | - | Impervious | 98 | 22.09 | 2164.39 | |
| CN ₂ | В | Managed Turf | 61 | 7.75 | 472.64 | |
| CN ₃ | С | Managed Turf | 74 | 31.99 | 2367.60 | |
| CN_4 | D | Managed Turf | 80 | 0.07 | 5.41 | |
| CN ₅ | В | Brush (Good) | 48 | 0.00 | 0.00 | |
| CN ₆ | С | Brush (Good) | 65 | 0.00 | 0.00 | |
| CN ₇ | D | Brush (Good) | 73 | 2.34 | 171.16 | |
| CN ₈ | | | | | 0.00 | |
| CN ₉ | | | | | 0.00 | |
| CN ₁₀ | | | | | 0.00 | |
| | | | Total | 64.24 | 5181.21 | |
| | | | Со | mposite CN = | 81 | |

| | Time of Concentration, T _c | | | | | | | |
|--------------|---------------------------------------|-----------------------|--------------|---------------|-----------------------------|-----------------------------|--|--|
| | | 2 yr. Precip. (in.) = | 2.73 | | | | | |
| | | | | Roughness | | Travel Time, T _t | | |
| Flow Segment | Flow Regime | Land Cover | Length (ft) | Coeff., n | Slope (ft/ft) | (min.) | | |
| 1 | Sheet Flow | Grass | 100 | 0.24 | 0.022 | 14.9 | | |
| 2 | Shallow Conc. | Unpaved | 452 | | 0.086 | 1.6 | | |
| 3 | Channel | Concrete | 244 | 0.013 | 0.029 | 0.5 | | |
| 4 | Channel | 30" Concrete Pipe | 1238 | 0.013 | 0.028 | 2.4 | | |
| 5 | | | | | | | | |
| 6 | | | | | | | | |
| 7 | | | | | | | | |
| 8 | | | | | | | | |
| 9 | | | | | | | | |
| 10 | | | | | | | | |
| | | | Total Time o | f Concentrati | on, T _c (min.) = | 19.3 | | |

| Runoff | | | | | | |
|--|-------|--------|---------|--|--|--|
| | 1 Yr. | 10 Yr. | 100 Yr. | | | |
| Precipitation (in.), P | 2.26 | 4.06 | 6.44 | | | |
| Composite CN | 81 | 81 | 81 | | | |
| Storage (in.) S=1000/CN-10 | 2.35 | 2.35 | 2.35 | | | |
| Initial abstraction (in.), I _a =0.2S | 0.47 | 0.47 | 0.47 | | | |
| Runoff depth (in.), Q=(P-0.2S) ² /[(P-I _a)+S] | 0.78 | 2.17 | 4.29 | | | |
| Runoff volume (ac-ft), RV = Q/12*A | 4.15 | 11.63 | 22.95 | | | |
| Flow rate (cfs), q _{peak} from hydrograph | 55.43 | 161.91 | | | | |
| Hudrograph Number | 2 | | | | | |

Hydrograph Number: 2

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 2

To 460 North Culvert (excluding Union)

| CS Runoff | Peak discharge = | 55.43 cfs |
|-----------|---|--|
| yrs | Time to peak = | • 726 min |
| min | Hyd. volume = | 180,801 cuft |
| 4.240 ac | Curve number = | : 81 |
| .0 % | Hydraulic length = | • 0 ft |
| ser | Time of conc. (Tc) = | : 19.30 min |
| .26 in | Distribution = | ∶ Type II |
| 4 hrs | Shape factor = | 484 |
| | CS Runoff yrs min 240 ac 0 % ser 26 in 4 hrs | CS RunoffPeak discharge=yrsTime to peak=minHyd. volume=4.240 acCurve number=0 %Hydraulic length=serTime of conc. (Tc)=26 inDistribution=4 hrsShape factor= |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Friday, 04 / 29 / 2022

Hyd. No. 2

To 460 North Culvert (excluding Union)

| Hydrograph type = | SCS Runoff | Peak discharge | = 161.91 cfs |
|-------------------|------------|--------------------|----------------|
| Storm frequency = | 10 yrs | Time to peak | = 724 min |
| Time interval = | 2 min | Hyd. volume | = 506,496 cuft |
| Drainage area = | 64.240 ac | Curve number | = 81 |
| Basin Slope = | 0.0 % | Hydraulic length | = 0 ft |
| Tc method = | User | Time of conc. (Tc) | = 19.30 min |
| Total precip. = | 4.06 in | Distribution | = Type II |
| Storm duration = | 24 hrs | Shape factor | = 484 |







12.02.2020 DATE 12/2/2020

Not to scale NOT FOR CONSTRUCTION

WORKSHEET FOR SCS HYDROLOGIC PARAMETERS

| Site Conditions: | Existing X Proposed | Project: Sturbridge Apartments Subarea Number: 1b Bypass - No Detention |
|--------------------|------------------------|---|
| | Existing | By: Justin Brown |
| Off-Site Land Use: | X Proposed | Date: 4/13/2020 |

RUNOFF CURVE NUMBER

| Soil Group | | Land Use or Zoning | Area (acres) | RCN | RCN x Area |
|---------------|---------|--------------------|-----------------|-----|---------------|
| В | On-Site | Impervious | 0.00 | 98 | 0.098 |
| В | On-Site | Open Space | 0.25 | 61 | 15.25 |
| С | On-Site | Impervious | 0.00 | 98 | 0 |
| С | On-Site | Open Space | 0.42 | 74 | 31.08 |
| D | On-Site | Impervious | 0.00 | 80 | 0 |
| D | On-Site | Open Space | 0.00 | 80 | 0 |
| | | | | | |
| | | | | | |

Total Area

0.001 sq. mi

Weighted RCN =

69

Notes:

0.67

ac

Time of Concentration = 8.28 minutes (See Attached)

| TR 55 Worksheet: Time of Concentration (Tc) | PROJEC | PROJECT: TNHSE19001 | | | PN: (Post-DEVELOPMENT: PO | | |
|---|---------------|---------------------|----------|----------|---------------------------|----------|----------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 6 |
| Sheet Flow | | 1 | | 1 A. | | | |
| Surface description (Table 3-1) | Dense Grasses | | | | | | |
| Manning's roughness coeff., n (Table 3-1) | 0.24 | | | | | 1 | |
| Flow length, L (total L < 100 ft) ft | 100.00 | | | 1 | Sec. 14 | 1 | |
| Two-year 24-hour rainfall, P2 in | 2.74 | | | | | | |
| Land slope, S ft/ft | 0.1500 | | 1 | | | | |
| $T_t = (0.007 (nL)^{0.8}) / (P_2^{0.5} s^{0.4}) \dots hr$ | 0.11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Shallow Concetrated Flow | | - | | | | | |
| Surface description (paved=1 or unpaved=0) | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Flow length, L ft | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Watercourse slope, S ft/ft | 0.0180 | 0.0100 | 0.0100 | 0.0100 | 0.0100 | 0.0100 | 0.0100 |
| Average velocity, V ft/s | - | | | - | - | - | - |
| Unpaved V = $16.1345 (s)^{0.5}$ | 2.16 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 |
| Paved $V = 20.3282 (s)^{0.5}$ | | | | | | | |
| T _t = L /3600Vhr | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Channel Flow | CHANNEL | 1 | | | | | |
| Cross sectional flow area, A ft ² | 3.00 | | | 1 | 1 | | |
| Wetted perimeter, Pw ft | 6.00 | | | | | | |
| Hydraulic radius, r = A/Pwft | 0.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Channel slope, s ft/ft | 0.068 | | | | | | |
| Vanning's roughness coefficient, n | 0.070 | 0.035 | 0.069 | 0.013 | 0.013 | 0.013 | 0.013 |
| /elocity, V=(1.49/n)R ^{2/3} s ^{1/2} ft | 3.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Flow length, L ft | 293.0 | | | | | | |
| Γ _t = L/3600Vhr | 0.023 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| Sub Basin Tc = $T_{sheetflow}+T_{shallow concentrated}+T_{channel}$ | 0.14 hr | 0.00 hr | 0.00 hr | 0.00 hr | 0.00 hr | 0.00 hr | 0.00 hr |
| Sub Basin Tc = $T_{sheetflow} + T_{shallow concentrated} + T_{channel} =$ | 8.28 min | 0.00 min | 0.00 min | 0.00 min | 0.00 min | 0.00 min | 0.00 min |

8.28 min

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 3

Union Bypass To 460 N Culvert



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 3

Union Bypass To 460 N Culvert

| Hydrograph type | = SCS Runoff | Peak discharge | = 1.371 cfs |
|-----------------|--------------|--------------------|--------------|
| Storm frequency | = 10 yrs | Time to peak | = 720 min |
| Time interval | = 2 min | Hyd. volume | = 3,176 cuft |
| Drainage area | = 0.670 ac | Curve number | = 69 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 8.30 min |
| Total precip. | = 4.06 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



WORKSHEET FOR SCS HYDROLOGIC PARAMETERS

| Site Conditions: | ExistingXProposed | Project: Sturbridge Apartments Subarea Number: 1a Detention | |
|--------------------|-------------------|---|---|
| | Existing | By: Justin Brown | _ |
| Off-Site Land Use: | X Proposed | Date: 4/13/2020 | |

RUNOFF CURVE NUMBER

| Group | | Land Use or Zoning | Area (acres) | RCN | RCN x Area |
|-------|---------|--------------------|-----------------|-----|---------------|
| В | On-Site | Impervious | 1.54 | 0.9 | 150.00 |
| В | On-Site | Open Space | 0.45 | 90 | 150.92 |
| С | On-Site | Impervious | 0.45 | 00 | 27.45 |
| С | On-Site | Open Space | 2.70 | 90 | 270.48 |
| D | On-Site | Impervious | 1.00 | 74 | 79.55 |
| D | On-Site | Open Space | 0.00 | 80 | 0 |
| | | | | | 1 |
| | | | | | |
| | | | | | |

Total Area 5.83

0.009 sq. mi

Weighted RCN =

91

Notes:

ac

Time of Concentration = 13.63 minutes (See Attached)

| TR 55 Worksheet: Time of Concentration (Tc) | PROJEC | T: TNHSE190 | 01 | PN: (Post-DEVELOPMENT: PO/ | | | POA#1 (| |
|---|---------------|-------------|----------|----------------------------|----------|------------|----------|----|
| | 1 | 2 | 3 | 4 | 5 | 6 | 6 |] |
| Sheet Flow | | | | | | | | 1 |
| Surface description (Table 3-1) | Dense Grasses | | 1 | | | | | 1 |
| Manning's roughness coeff., n (Table 3-1) | 0.24 | | | | | the second | | |
| Flow length, L (total L < 100 ft) ft | 100.00 | | 1 | | | 1.000 | | 1 |
| Two-year 24-hour rainfall, P2 in | 2.74 | | | | | | | 1 |
| Land slope, S ft/ft | 0.0880 | | | | 1 | | 1 | 1 |
| $T_t = (0.007 (nL)^{0.8}) / (P_2^{0.5} s^{0.4}) \dots hr$ | 0.14 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1 |
| Shallow Concetrated Flow | | | | | | | | 1 |
| Surface description (paved=1 or unpaved=0) | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| Flow length, L ft | 155.0 | 190.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1 |
| Watercourse slope, S ft/ft | 0.0840 | 0.0210 | 0.0100 | 0.0100 | 0.0100 | 0.0100 | 0.0100 | 1 |
| Average velocity, V ft/s | | | | • | | - | | |
| Unpaved V = 16.1345 (s) ^{0.5} | 4.68 | | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 | 1 |
| Paved $V = 20.3282 (s)^{0.5}$ | | 2.95 | | | | | 16 | 1 |
| T _t = L /3600V hr | 0.01 | 0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1 |
| Channel Flow | CHANNEL | | | | | | | 1 |
| Cross sectional flow area, A ft ² | 3.10 | | | | | | | 1 |
| Wetted perimeter, Pw ft | 6.30 | | | | | | | |
| Hydraulic radius, r = A/Pwft | 0.49 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |] |
| Channel slope, s ft/ft | 0.010 | | | | 1 | | | |
| Manning's roughness coefficient, n | 0.045 | 0.035 | 0.069 | 0.013 | 0.013 | 0.013 | 0.013 | |
| Velocity, V=(1.49/n)R ^{2/3} s ^{1/2} ft | 2.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Flow length, L ft | 431.0 | | | | | | | 10 |
| T _t = L/3600V hr | 0.058 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| Sub Basin Tc = $T_{sheetflow} + T_{shallow concentrated} + T_{channel} =$ | 0.21 hr | 0.02 hr | 0.00 hr | 0.00 hr | 0.00 hr | 0.00 hr | 0.00 hr | |
| Sub Basin Tc = T _{sheetflow} +T _{shallow} concentrated+T _{channel} = | 12.56 min | 1.07 min | 0.00 min | 0.00 min | 0.00 min | 0.00 min | 0.00 min | 13 |

13:63 min

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 4

Union North Detention inflow

| Hydrograph type | = SCS Runoff | Peak discharge | = 10.22 cfs |
|-----------------|--------------|--------------------|---------------|
| Storm frequency | = 1 yrs | Time to peak | = 722 min |
| Time interval | = 2 min | Hyd. volume | = 28,759 cuft |
| Drainage area | = 5.830 ac | Curve number | = 91 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 13.60 min |
| Total precip. | = 2.26 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 4

Union North Detention inflow

| Hydrograph type | = SCS Runoff | Peak discharge | = 21.90 cfs |
|-----------------|--------------|--------------------|---------------|
| Storm frequency | = 10 yrs | Time to peak | = 722 min |
| Time interval | = 2 min | Hyd. volume | = 63,445 cuft |
| Drainage area | = 5.830 ac | Curve number | = 91 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 13.60 min |
| Total precip. | = 4.06 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Pond No. 10 - Union North Underground Det.

Pond Data

UG Chambers -Invert elev. = 2041.00 ft, Rise x Span = 4.00×4.00 ft, Barrel Len = 204.00 ft, No. Barrels = 5, Slope = 0.50%, Headers = Yes **Encasement -**Invert elev. = 2040.50 ft, Width = 6.50 ft, Height = 5.50 ft, Voids = 40.00%

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 2040.50 | n/a | 0 | 0 |
| 0.65 | 2041.15 | n/a | 613 | 613 |
| 1.30 | 2041.80 | n/a | 2,016 | 2,629 |
| 1.96 | 2042.46 | n/a | 2,971 | 5,600 |
| 2.61 | 2043.11 | n/a | 3,384 | 8,985 |
| 3.26 | 2043.76 | n/a | 3,509 | 12,493 |
| 3.91 | 2044.41 | n/a | 3,432 | 15,925 |
| 4.56 | 2045.06 | n/a | 3,103 | 19,028 |
| 5.22 | 2045.72 | n/a | 2,379 | 21,407 |
| 5.87 | 2046.37 | n/a | 1,893 | 23,300 |
| 6.52 | 2047.02 | n/a | 1,840 | 25,140 |

Culvert / Orifice Structures

Weir Structures

| | [A] | [B] | [C] | [PrfRsr] | | [A] | [B] | [C] | [D] |
|-----------------|-----------|---------|---------|----------|----------------|-------------|-----------|------|------|
| Rise (in) | = 30.00 | 7.00 | 5.00 | 0.00 | Crest Len (ft) | = 18.85 | 0.33 | 0.00 | 0.00 |
| Span (in) | = 30.00 | 8.25 | 72.00 | 0.00 | Crest El. (ft) | = 2047.52 | 2045.20 | 0.00 | 0.00 |
| No. Barrels | = 1 | 1 | 1 | 0 | Weir Coeff. | = 3.33 | 3.33 | 3.33 | 3.33 |
| Invert El. (ft) | = 2041.00 | 2041.00 | 2043.50 | 0.00 | Weir Type | = 1 | Rect | | |
| Length (ft) | = 30.00 | 0.00 | 0.00 | 0.00 | Multi-Stage | = Yes | Yes | No | No |
| Slope (%) | = 2.00 | 0.00 | 0.00 | n/a | | | | | |
| N-Value | = .013 | .013 | .013 | n/a | | | | | |
| Orifice Coeff. | = 0.60 | 0.60 | 0.60 | 0.60 | Exfil.(in/hr) | = 0.000 (by | Wet area) | | |
| Multi-Stage | = n/a | Yes | Yes | No | TW Elev. (ft) | = 0.00 | | | |

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s). Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| 0.00 | 0 | 2040.50 | 0.00 | 0.00 | 0.00 | | 0.00 | 0.00 | | | | | 0.000 |
| 0.07 | 61 | 2040.56 | 0.00 | 0.00 | 0.00 | | 0.00 | 0.00 | | | | | 0.000 |
| 0.13 | 123 | 2040.63 | 0.00 | 0.00 | 0.00 | | 0.00 | 0.00 | | | | | 0.000 |
| 0.20 | 184 | 2040.70 | 0.00 | 0.00 | 0.00 | | 0.00 | 0.00 | | | | | 0.000 |
| 0.26 | 245 | 2040.76 | 0.00 | 0.00 | 0.00 | | 0.00 | 0.00 | | | | | 0.000 |
| 0.33 | 307 | 2040.83 | 0.00 | 0.00 | 0.00 | | 0.00 | 0.00 | | | | | 0.000 |
| 0.39 | 368 | 2040.89 | 0.00 | 0.00 | 0.00 | | 0.00 | 0.00 | | | | | 0.000 |
| 0.46 | 429 | 2040.96 | 0.00 | 0.00 | 0.00 | | 0.00 | 0.00 | | | | | 0.000 |
| 0.52 | 491 | 2041.02 | 0.00 ic | 0.00 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.003 |
| 0.59 | 552 | 2041.09 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.038 |
| 0.65 | 613 | 2041.15 | 0.10 ic | 0.10 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.098 |
| 0.72 | 815 | 2041.22 | 0.18 ic | 0.18 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.180 |
| 0.78 | 1,017 | 2041.28 | 0.29 ic | 0.28 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.277 |
| 0.85 | 1,218 | 2041.35 | 0.39 ic | 0.39 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.391 |
| 0.91 | 1,420 | 2041.41 | 0.52 ic | 0.52 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.517 |
| 0.98 | 1,621 | 2041.48 | 0.66 ic | 0.66 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.663 |
| 1.04 | 1,823 | 2041.54 | 0.84 ic | 0.81 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.812 |
| 1.11 | 2,025 | 2041.61 | 0.97 ic | 0.95 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.950 |
| 1.17 | 2,226 | 2041.67 | 1.04 ic | 1.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.044 |
| 1.24 | 2,428 | 2041.74 | 1.13 ic | 1.12 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.125 |
| 1.30 | 2,629 | 2041.80 | 1.21 ic | 1.21 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.206 |
| 1.37 | 2,926 | 2041.87 | 1.29 ic | 1.29 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.285 |
| 1.43 | 3,224 | 2041.93 | 1.37 ic | 1.36 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.360 |
| 1.50 | 3,521 | 2042.00 | 1.46 ic | 1.43 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.427 |
| 1.56 | 3,818 | 2042.06 | 1.55 ic | 1.49 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.491 |
| 1.63 | 4,115 | 2042.13 | 1.56 ic | 1.56 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.564 |
| 1.70 | 4,412 | 2042.19 | 1.65 ic | 1.63 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.628 |
| 1.76 | 4,709 | 2042.26 | 1.76 ic | 1.68 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.684 |
| 1.83 | 5.006 | 2042.32 | 1.76 ic | 1.75 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.755 |
| 1.89 | 5,303 | 2042.39 | 1.86 ic | 1.81 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.807 |
| 1.96 | 5,600 | 2042.46 | 1.87 ic | 1.87 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.869 |
| 2.02 | 5,939 | 2042.52 | 1.97 ic | 1.92 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.921 |
| | 3,000 | | | | | | | | | | | | |

Union North Underground Det. Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|--------------|------------------|--------------------|----------------------|--------------------|----------------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| 2.09 | 6,277 | 2042.59 | 1.98 ic | 1.98 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.980 |
| 2.15 | 6,616 | 2042.65 | 2.09 ic | 2.03 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.029 |
| 2.22 | 6,954 | 2042.72 | 2.09 ic | 2.09 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.088 |
| 2.28 | 7,292 | 2042.78 | 2.21 ic | 2.13 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.131 |
| 2.35 | 7,631 | 2042.85 | 2.21 ic | 2.19 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.188 |
| 2.41 | 7,969 | 2042.91 | 2.23 ic | 2.23 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.232 |
| 2.48 | 8,308 | 2042.98 | 2.33 ic | 2.28 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.283 |
| 2.54 | 8,646 | 2043.04 | 2.33 IC | 2.33 IC | 0.00 | | 0.00 | 0.00 | | | | | 2.334 |
| 2.01 | 8,985 | 2043.11 | 2.46 IC | 2.37 IC | 0.00 | | 0.00 | 0.00 | | | | | 2.374 |
| 2.07 | 9,335 | 2043.17 | 2.40 IC | 2.42 IC 2.47 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.424 |
| 2.74 | 9,000 | 2043.24 | 2.47 IC 2.59 ic | 2.47 IC 2.51 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.470 |
| 2.00 | 10,007 | 2043.37 | 2.50 ic | 2.51 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.510 |
| 2.07 | 10,000 | 2043 43 | 2.00 ic | 2.00 ic | 0.00 | | 0.00 | 0.00 | | | | | 2 602 |
| 3.00 | 11.090 | 2043.50 | 2.73 ic | 2.64 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.639 |
| 3.06 | 11,441 | 2043.56 | 3.02 ic | 2.66 ic | 0.33 ic | | 0.00 | 0.00 | | | | | 2.994 |
| 3.13 | 11,791 | 2043.63 | 3.64 ic | 2.66 ic | 0.95 ic | | 0.00 | 0.00 | | | | | 3.610 |
| 3.19 | 12,142 | 2043.69 | 4.52 ic | 2.64 ic | 1.76 ic | | 0.00 | 0.00 | | | | | 4.394 |
| 3.26 | 12,493 | 2043.76 | 5.33 ic | 2.62 ic | 2.71 ic | | 0.00 | 0.00 | | | | | 5.333 |
| 3.33 | 12,836 | 2043.82 | 6.39 ic | 2.60 ic | 3.79 ic | | 0.00 | 0.00 | | | | | 6.393 |
| 3.39 | 13,180 | 2043.89 | 7.56 ic | 2.58 ic | 4.98 ic | | 0.00 | 0.00 | | | | | 7.562 |
| 3.46 | 13,523 | 2043.96 | 8.55 ic | 2.57 ic | 5.99 ic | | 0.00 | 0.00 | | | | | 8.554 |
| 3.52 | 13,866 | 2044.02 | 9.31 ic | 2.58 ic | 6.73 ic | | 0.00 | 0.00 | | | | | 9.305 |
| 3.59 | 14,209 | 2044.09 | 10.06 ic | 2.59 ic | 7.40 ic | | 0.00 | 0.00 | | | | | 9.985 |
| 3.65 | 14,552 | 2044.15 | 10.61 ic | 2.60 IC | 8.01 IC | | 0.00 | 0.00 | | | | | 10.61 |
| 3.72 | 14,896 | 2044.22 | 11.19 IC | 2.62 IC | 8.58 IC | | 0.00 | 0.00 | | | | | 11.19 |
| 3.78 | 15,239 | 2044.28 | 11.75 IC 12.27 io | 2.03 IC | 9.11 IC | | 0.00 | 0.00 | | | | | 11.75 |
| 3.00 | 15,002 | 2044.33 | 12.27 IC | 2.00 IC 2.68 ic | 9.02 IC | | 0.00 | 0.00 | | | | | 12.27 |
| 3.98 | 16 236 | 2044.41 | 13 35 ic | 2.00 ic 2.70 ic | 10.10 ic | | 0.00 | 0.00 | | | | | 13.25 |
| 4 04 | 16,546 | 2044 54 | 13.91 ic | 2.70 ic | 10.99 ic | | 0.00 | 0.00 | | | | | 13 71 |
| 4 11 | 16,856 | 2044 61 | 14 19 ic | 2.72 ic | 11 41 ic | | 0.00 | 0.00 | | | | | 14 16 |
| 4.17 | 17,166 | 2044.67 | 14.74 ic | 2.77 ic | 11.82 ic | | 0.00 | 0.00 | | | | | 14.59 |
| 4.24 | 17,477 | 2044.74 | 15.02 ic | 2.80 ic | 12.21 ic | | 0.00 | 0.00 | | | | | 15.01 |
| 4.30 | 17,787 | 2044.80 | 15.57 ic | 2.82 ic | 12.59 ic | | 0.00 | 0.00 | | | | | 15.41 |
| 4.37 | 18,097 | 2044.87 | 15.85 ic | 2.85 ic | 12.96 ic | | 0.00 | 0.00 | | | | | 15.81 |
| 4.43 | 18,408 | 2044.93 | 16.19 ic | 2.87 ic | 13.32 ic | | 0.00 | 0.00 | | | | | 16.19 |
| 4.50 | 18,718 | 2045.00 | 16.66 ic | 2.90 ic | 13.67 ic | | 0.00 | 0.00 | | | | | 16.57 |
| 4.56 | 19,028 | 2045.06 | 16.94 ic | 2.93 ic | 14.02 ic | | 0.00 | 0.00 | | | | | 16.94 |
| 4.63 | 19,266 | 2045.13 | 17.46 ic | 2.95 ic | 14.35 ic | | 0.00 | 0.00 | | | | | 17.30 |
| 4.69 | 19,504 | 2045.19 | 17.72 IC | 2.98 IC | 14.67 IC | | 0.00 | 0.00 | | | | | 17.65 |
| 4.76 | 19,742 | 2045.26 | 18.01 IC | 3.00 IC | 14.99 IC | | 0.00 | 0.02 | | | | | 18.01 |
| 4.02 | 19,900 | 2045.32 | 10.50 IC | 3.03 IC 2.05 io | 15.30 IC | | 0.00 | 0.05 | | | | | 10.30 |
| 4.09 | 20,210 | 2045.39 | 10.70 IC | 3.05 iC 3.07 ic | 15.01 ic | | 0.00 | 0.09 | | | | | 10.70 |
| 5.02 | 20,430 | 2045.45 | 19.24 iC | 3.07 ic | 16.20 ic | | 0.00 | 0.14 | | | | | 10.10 |
| 5.02 | 20,034 | 2045.58 | 20.01 oc | 3 11 ic | 16 49 ic | | 0.00 | 0.20 | | | | | 19.87 |
| 5.15 | 21,169 | 2045.65 | 20.30 oc | 3.13 ic | 16.78 ic | | 0.00 | 0.33 | | | | | 20.24 |
| 5.22 | 21,407 | 2045.72 | 20.71 oc | 3.15 ic | 17.06 ic | | 0.00 | 0.41 | | | | | 20.61 |
| 5.28 | 21,597 | 2045.78 | 21.08 oc | 3.16 ic | 17.33 ic | | 0.00 | 0.49 | | | | | 20.98 |
| 5.35 | 21,786 | 2045.85 | 21.42 oc | 3.17 ic | 17.60 ic | | 0.00 | 0.57 | | | | | 21.34 |
| 5.41 | 21,975 | 2045.91 | 21.72 oc | 3.19 ic | 17.87 ic | | 0.00 | 0.66 | | | | | 21.71 |
| 5.48 | 22,164 | 2045.98 | 22.15 oc | 3.19 ic | 18.13 ic | | 0.00 | 0.75 | | | | | 22.07 |
| 5.54 | 22,354 | 2046.04 | 22.48 oc | 3.19 ic | 18.39 ic | | 0.00 | 0.85 | | | | | 22.43 |
| 5.61 | 22,543 | 2046.11 | 22.80 oc | 3.19 ic | 18.64 ic | | 0.00 | 0.95 | | | | | 22.79 |
| 5.67 | 22,732 | 2046.17 | 23.10 oc | 3.15 ic | 18.89 ic | | 0.00 | 1.05 | | | | | 23.10 |
| 5.74 | 22,921 | 2046.24 | 23.48 oc | 3.18 IC | 19.14 ic | | 0.00 | 1.16 | | | | | 23.48 |
| 5.80 | 23,111 | 2046.30 | 23.87 oc | 3.20 IC | 19.39 IC | | 0.00 | 1.27 | | | | | 23.86 |
| 5.87 | 23,300 | 2046.37 | 24.25 OC | 3.23 IC 2.25 io | 19.63 IC | | 0.00 | 1.39 | | | | | 24.20 |
| 0.90 6.00 | 23,404 | 2040.43 20/6 50 | 24.00 00 | 3.20 IC | 19.07 IC 20.11 in | | 0.00 | 1.01 | | | | | 24.03 |
| 6.00 | 23,000 23 852 | 2040.00 | 25.01.00 | 3.20 IC | 20.1110 20.3/1 ic | | 0.00 | 1.03 | | | | | 25.01 |
| 6.13 | 23,032 | 2046.63 | 25.78 00 | 3.33 ic | 20.04 iC | | 0.00 | 1.88 | | | | | 25.59 |
| 6 19 | 24 220 | 2046 69 | 26 16 00 | 3.35 ic | 20.80 ic | | 0.00 | 2 01 | | | | | 26.16 |
| 6.26 | 24,404 | 2046.76 | 26.54 oc | 3.37 ic | 21.03 ic | | 0.00 | 2.14 | | | | | 26.54 |
| 6.32 | 24,588 | 2046.82 | 26.86 oc | 3.40 ic | 21.19 ic | | 0.00 | 2.28 | | | | | 26.86 |
| 6.39 | 24,772 | 2046.89 | 27.18 oc | 3.42 ic | 21.34 ic | | 0.00 | 2.41 | | | | | 27.18 |
| 6.45 | 24,956 | 2046.95 | 27.50 oc | 3.45 ic | 21.50 ic | | 0.00 | 2.55 | | | | | 27.50 |
| 6.52 | 25,140 | 2047.02 | 27.82 oc | 3.47 ic | 21.65 ic | | 0.00 | 2.70 | | | | | 27.82 |

...End

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Friday, 04 / 29 / 2022

Hyd. No. 5

Union N. Basin Out

| Hydrograph type | = Reservoir | Peak discharge | = 2.591 cfs |
|-----------------|-----------------------------------|----------------|---------------|
| Storm frequency | = 1 yrs | Time to peak | = 738 min |
| Time interval | = 2 min | Hyd. volume | = 28,310 cuft |
| Inflow hyd. No. | = 4 - Union North Detention inflo | Max. Elevation | = 2043.42 ft |
| Reservoir name | = Union North Underground Det | .Max. Storage | = 10,652 cuft |

Storage Indication method used.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Friday, 04 / 29 / 2022

Hyd. No. 5

Union N. Basin Out

| Hydrograph type | = Reservoir | Peak discharge | = 14.58 cfs |
|-----------------|-----------------------------------|----------------|---------------|
| Storm frequency | = 10 yrs | Time to peak | = 730 min |
| Time interval | = 2 min | Hyd. volume | = 62,997 cuft |
| Inflow hyd. No. | = 4 - Union North Detention inflo | Max. Elevation | = 2044.67 ft |
| Reservoir name | = Union North Underground Det | .Max. Storage | = 17,158 cuft |

Storage Indication method used.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 6

Total To 460 North Culvert

| Hydrograph type | = Combine | Peak discharge | = 57.90 cfs |
|-----------------|-----------|----------------------|----------------|
| Storm frequency | = 1 yrs | Time to peak | = 726 min |
| Time interval | = 2 min | Hyd. volume | = 209,881 cuft |
| Inflow hyds. | = 2, 3, 5 | Contrib. drain. area | = 64.910 ac |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 6

Total To 460 North Culvert

| Hydrograph type | = Combine | Peak discharge | = 175.44 cfs |
|-----------------|-----------|----------------------|----------------|
| Storm frequency | = 10 yrs | Time to peak | = 724 min |
| Time interval | = 2 min | Hyd. volume | = 572,669 cuft |
| Inflow hyds. | = 2, 3, 5 | Contrib. drain. area | = 64.910 ac |



Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Pond No. 8 - 460 North Culvert HW Storage

Pond Data

Contours -User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 2033.00 ft

Stage / Storage Table

| Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|----------------|--|--|--|
| 2033.00 | 00 | 0 | 0 |
| 2035.00 | 271 | 271 | 271 |
| 2036.00 | 997 | 634 | 905 |
| 2037.00 | 1,787 | 1,392 | 2,297 |
| 2038.00 | 3,429 | 2,608 | 4,905 |
| 2039.00 | 4,748 | 4,089 | 8,994 |
| 2040.00 | 7,034 | 5,891 | 14,885 |
| 2041.00 | 8,939 | 7,987 | 22,871 |
| 2042.00 | 11,317 | 10,128 | 32,999 |
| 2043.00 | 13,359 | 12,338 | 45,337 |
| 2044.00 | 15,556 | 14,458 | 59,795 |
| 2045.00 | 18,050 | 16,803 | 76,598 |
| | Elevation (ft) 2033.00 2035.00 2036.00 2037.00 2038.00 2040.00 2041.00 2041.00 2042.00 2043.00 2044.00 2045.00 | Elevation (ft)Contour area (sqft)2033.00002035.002712036.009972037.001,7872038.003,4292039.004,7482040.007,0342041.008,9392042.0011,3172043.0013,3592044.0015,5562045.0018,050 | Elevation (ft)Contour area (sqft)Incr. Storage (cuft)2033.000002035.002712712036.009976342037.001,7871,3922038.003,4292,6082039.004,7484,0892040.007,0345,8912041.008,9397,9872042.0011,31710,1282043.0013,35912,3382044.0015,55614,4582045.0018,05016,803 |

Culvert / Orifice Structures

Weir Structures

| | [A] | [B] | [C] | [PrfRsr] | | [A] | [B] | [C] | [D] |
|-----------------|-----------|------|------|----------|----------------|-------------|------------|------|------|
| Rise (in) | = 48.00 | 0.00 | 0.00 | 0.00 | Crest Len (ft) | = 0.00 | 0.00 | 0.00 | 0.00 |
| Span (in) | = 48.00 | 0.00 | 0.00 | 0.00 | Crest El. (ft) | = 0.00 | 0.00 | 0.00 | 0.00 |
| No. Barrels | = 1 | 0 | 0 | 0 | Weir Coeff. | = 3.33 | 3.33 | 3.33 | 3.33 |
| Invert El. (ft) | = 2033.10 | 0.00 | 0.00 | 0.00 | Weir Type | = | | | |
| Length (ft) | = 160.50 | 0.00 | 0.00 | 0.00 | Multi-Stage | = No | No | No | No |
| Slope (%) | = 2.69 | 0.00 | 0.00 | n/a | - | | | | |
| N-Value | = .024 | .013 | .013 | n/a | | | | | |
| Orifice Coeff. | = 0.60 | 0.60 | 0.60 | 0.60 | Exfil.(in/hr) | = 0.000 (by | (Wet area) | | |
| Multi-Stage | = n/a | No | No | No | TW Elev. (ft) | = 0.00 | , | | |

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s). Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| 0.00 | 0 | 2033.00 | 0.00 | | | | | | | | | | 0.000 |
| 0.20 | 27 | 2033.20 | 0.09 ic | | | | | | | | | | 0.091 |
| 0.40 | 54 | 2033.40 | 0.80 ic | | | | | | | | | | 0.804 |
| 0.60 | 81 | 2033.60 | 2.19 ic | | | | | | | | | | 2.195 |
| 0.80 | 108 | 2033.80 | 4.22 ic | | | | | | | | | | 4.217 |
| 1.00 | 136 | 2034.00 | 6.86 ic | | | | | | | | | | 6.857 |
| 1.20 | 163 | 2034.20 | 10.03 ic | | | | | | | | | | 10.03 |
| 1.40 | 190 | 2034.40 | 13.78 ic | | | | | | | | | | 13.78 |
| 1.60 | 217 | 2034.60 | 17.99 ic | | | | | | | | | | 17.99 |
| 1.80 | 244 | 2034.80 | 22.63 ic | | | | | | | | | | 22.63 |
| 2.00 | 271 | 2035.00 | 27.66 ic | | | | | | | | | | 27.66 |
| 2.10 | 334 | 2035.10 | 30.31 ic | | | | | | | | | | 30.31 |
| 2.20 | 398 | 2035.20 | 32.98 ic | | | | | | | | | | 32.98 |
| 2.30 | 461 | 2035.30 | 35.78 ic | | | | | | | | | | 35.78 |
| 2.40 | 525 | 2035.40 | 38.63 ic | | | | | | | | | | 38.63 |
| 2.50 | 588 | 2035.50 | 41.58 ic | | | | | | | | | | 41.58 |
| 2.60 | 651 | 2035.60 | 44.49 ic | | | | | | | | | | 44.49 |
| 2.70 | 715 | 2035.70 | 47.47 ic | | | | | | | | | | 47.47 |
| 2.80 | 778 | 2035.80 | 50.51 ic | | | | | | | | | | 50.51 |
| 2.90 | 842 | 2035.90 | 53.53 ic | | | | | | | | | | 53.53 |
| 3.00 | 905 | 2036.00 | 56.62 ic | | | | | | | | | | 56.62 |
| 3.10 | 1,044 | 2036.10 | 59.65 ic | | | | | | | | | | 59.65 |
| 3.20 | 1,183 | 2036.20 | 62.66 ic | | | | | | | | | | 62.66 |
| 3.30 | 1,323 | 2036.30 | 65.66 ic | | | | | | | | | | 65.66 |
| 3.40 | 1,462 | 2036.40 | 68.61 ic | | | | | | | | | | 68.61 |
| 3.50 | 1,601 | 2036.50 | 71.49 ic | | | | | | | | | | 71.49 |
| 3.60 | 1,740 | 2036.60 | 74.27 ic | | | | | | | | | | 74.27 |
| 3.70 | 1,879 | 2036.70 | 76.97 ic | | | | | | | | | | 76.97 |
| 3.80 | 2,019 | 2036.80 | 79.50 ic | | | | | | | | | | 79.50 |
| 3.90 | 2,158 | 2036.90 | 81.85 ic | | | | | | | | | | 81.85 |
| 4.00 | 2,297 | 2037.00 | 83.93 ic | | | | | | | | | | 83.93 |
| | - | | | | | | | | | | | | |

460 North Culvert HW Storage Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|-------------|------------------|-----------------|----------------------|--------------|--------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| 4.10 | 2,558 | 2037.10 | 85.56 ic | | | | | | | | | | 85.56 |
| 4.20 | 2,819 | 2037.20 | 87.67 ic | | | | | | | | | | 87.67 |
| 4.30 | 3,079 | 2037.30 | 89.74 ic | | | | | | | | | | 89.74 |
| 4.40 | 3,340 3,601 | 2037.40 | 91.75 IC 93.73 ic | | | | | | | | | | 91.75 |
| 4.50 | 3 862 | 2037.60 | 95.66 ic | | | | | | | | | | 95.66 |
| 4.70 | 4,123 | 2037.70 | 97.55 ic | | | | | | | | | | 97.55 |
| 4.80 | 4,383 | 2037.80 | 99.41 ic | | | | | | | | | | 99.41 |
| 4.90 | 4,644 | 2037.90 | 101.24 ic | | | | | | | | | | 101.24 |
| 5.00 | 4,905 | 2038.00 | 103.03 ic | | | | | | | | | | 103.03 |
| 5.10 | 5,314 | 2038.10 | 104.79 IC | | | | | | | | | | 104.79 |
| 5.20 | 6 132 | 2038.30 | 108.23 ic | | | | | | | | | | 108.32 |
| 5.40 | 6.540 | 2038.40 | 109.90 ic | | | | | | | | | | 109.90 |
| 5.50 | 6,949 | 2038.50 | 111.56 ic | | | | | | | | | | 111.56 |
| 5.60 | 7,358 | 2038.60 | 113.18 ic | | | | | | | | | | 113.18 |
| 5.70 | 7,767 | 2038.70 | 114.79 ic | | | | | | | | | | 114.79 |
| 5.80 | 8,176 | 2038.80 | 116.37 ic | | | | | | | | | | 116.37 |
| 5.90 | 8,585 | 2038.90 | 117.94 IC | | | | | | | | | | 117.94 |
| 6.00 | 0,994 | 2039.00 | 121 00 ic | | | | | | | | | | 121 00 |
| 6.20 | 10.172 | 2039.20 | 122.50 ic | | | | | | | | | | 121.00 |
| 6.30 | 10,761 | 2039.30 | 123.99 ic | | | | | | | | | | 123.99 |
| 6.40 | 11,350 | 2039.40 | 125.45 ic | | | | | | | | | | 125.45 |
| 6.50 | 11,939 | 2039.50 | 126.90 ic | | | | | | | | | | 126.90 |
| 6.60 | 12,528 | 2039.60 | 128.34 ic | | | | | | | | | | 128.34 |
| 6.70 | 13,117 | 2039.70 | 129.69 oc | | | | | | | | | | 129.69 |
| 0.80 | 13,700 | 2039.80 | 130.03 OC | | | | | | | | | | 130.03 |
| 7 00 | 14,295 | 2039.90 | 132 47 oc | | | | | | | | | | 132.47 |
| 7.10 | 15.683 | 2040.10 | 133.39 oc | | | | | | | | | | 133.39 |
| 7.20 | 16,482 | 2040.20 | 134.30 oc | | | | | | | | | | 134.30 |
| 7.30 | 17,280 | 2040.30 | 135.20 oc | | | | | | | | | | 135.20 |
| 7.40 | 18,079 | 2040.40 | 136.10 oc | | | | | | | | | | 136.10 |
| 7.50 | 18,878 | 2040.50 | 136.99 oc | | | | | | | | | | 136.99 |
| 7.60 | 19,676 | 2040.60 | 137.87 OC | | | | | | | | | | 137.87 |
| 7.70 | 20,475 | 2040.70 | 130.75 0C | | | | | | | | | | 130.75 |
| 7.90 | 22.072 | 2040.90 | 140.49 oc | | | | | | | | | | 140.49 |
| 8.00 | 22,871 | 2041.00 | 141.35 oc | | | | | | | | | | 141.35 |
| 8.10 | 23,884 | 2041.10 | 142.21 oc | | | | | | | | | | 142.21 |
| 8.20 | 24,897 | 2041.20 | 143.06 oc | | | | | | | | | | 143.06 |
| 8.30 | 25,909 | 2041.30 | 143.91 oc | | | | | | | | | | 143.91 |
| 8.40 | 26,922 | 2041.40 | 144.75 OC | | | | | | | | | | 144.75 |
| 8.60 | 27,935 | 2041.50 | 145.59 0C | | | | | | | | | | 145.59 |
| 8.70 | 29,961 | 2041.70 | 147.25 oc | | | | | | | | | | 147.25 |
| 8.80 | 30,973 | 2041.80 | 148.07 oc | | | | | | | | | | 148.07 |
| 8.90 | 31,986 | 2041.90 | 148.89 oc | | | | | | | | | | 148.89 |
| 9.00 | 32,999 | 2042.00 | 149.71 oc | | | | | | | | | | 149.71 |
| 9.10 | 34,233 | 2042.10 | 150.52 oc | | | | | | | | | | 150.52 |
| 9.20 | 35,467 | 2042.20 | 151.32 oc | | | | | | | | | | 151.32 |
| 9.30 | 30,700 | 2042.30 | 152.12.00 | | | | | | | | | | 152.12 |
| 9.40 | 39 168 | 2042.40 | 153 71 oc | | | | | | | | | | 153.92 |
| 9.60 | 40.402 | 2042.60 | 154.50 oc | | | | | | | | | | 154.50 |
| 9.70 | 41,636 | 2042.70 | 155.29 oc | | | | | | | | | | 155.29 |
| 9.80 | 42,869 | 2042.80 | 156.07 oc | | | | | | | | | | 156.07 |
| 9.90 | 44,103 | 2042.90 | 156.85 oc | | | | | | | | | | 156.85 |
| 10.00 | 45,337 | 2043.00 | 157.62 oc | | | | | | | | | | 157.62 |
| 10.10 | 40,783 | 2043.10 | 158.39 00 | | | | | | | | | | 158.39 |
| 10.20 | 49 674 | 2043.30 | 159.92 00 | | | | | | | | | | 159.10 |
| 10.40 | 51.120 | 2043.40 | 160.67 oc | | | | | | | | | | 160.67 |
| 10.50 | 52,566 | 2043.50 | 161.43 oc | | | | | | | | | | 161.43 |
| 10.60 | 54,012 | 2043.60 | 162.18 oc | | | | | | | | | | 162.18 |
| 10.70 | 55,457 | 2043.70 | 162.93 oc | | | | | | | | | | 162.93 |
| 10.80 | 56,903 | 2043.80 | 163.67 oc | | | | | | | | | | 163.67 |
| 10.90 | 58,349 50 705 | 2043.90 | 164.41 OC | | | | | | | | | | 165.15 |
| 11.00 | 61 475 | 2044.00 | 165.89 00 | | | | | | | | | | 165.15 |
| 11.20 | 63,155 | 2044.20 | 166.62 oc | | | | | | | | | | 166.62 |
| | , | | | | | | | | | | | | |

460 North Culvert HW Storage Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| 11.30 | 64,835 | 2044.30 | 167.35 oc | | | | | | | | | | 167.35 |
| 11.40 | 66,516 | 2044.40 | 168.07 oc | | | | | | | | | | 168.07 |
| 11.50 | 68,196 | 2044.50 | 168.79 oc | | | | | | | | | | 168.79 |
| 11.60 | 69.876 | 2044.60 | 169.51 oc | | | | | | | | | | 169.51 |
| 11.70 | 71,557 | 2044.70 | 170.23 oc | | | | | | | | | | 170.23 |
| 11.80 | 73,237 | 2044.80 | 170.94 oc | | | | | | | | | | 170.94 |
| 11.90 | 74,917 | 2044.90 | 171.65 oc | | | | | | | | | | 171.65 |
| 12.00 | 76,598 | 2045.00 | 172.36 oc | | | | | | | | | | 172.36 |
| | | | | | | | | | | | | | |

...End

60



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

460 North Culvert Out

| Hydrograph type | = Reservoir | Peak discharge | = 57.76 cfs |
|-----------------|-----------------------|----------------------------|----------------|
| Storm frequency | = 1 yrs | Time to peak | = 726 min |
| Time interval | = 2 min | Hyd. volume | = 209,881 cuft |
| Inflow hyd. No. | = 6 - Total To 460 No | rth Culvert Max. Elevation | = 2036.04 ft |
| Reservoir name | = 460 North Culvert H | IW StorageMax. Storage | = 957 cuft |

Storage Indication method used.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Friday, 04 / 29 / 2022

Hyd. No. 7

460 North Culvert Out

| Hydrograph type | = Reservoir | Peak discharge | = 144.96 cfs |
|-----------------|----------------------------------|----------------|----------------|
| Storm frequency | = 10 yrs | Time to peak | = 730 min |
| Time interval | = 2 min | Hyd. volume | = 572,669 cuft |
| Inflow hyd. No. | = 6 - Total To 460 North Culvert | Max. Elevation | = 2041.43 ft |
| Reservoir name | = 460 North Culvert HW Storage | eMax. Storage | = 27,173 cuft |

Storage Indication method used.



Drainage Area Runoff and Time of Concentration

| | PREDEVELOPIVIENT | | | | | | | |
|------------------|------------------|---------------------|-------|---------------|--------|------------------------------|--|--|
| | C | omposite Curve Numl | | | Notes: | | | |
| | Hydrologic Soil | | | | | | | |
| | Group | Land Cover | CN | Area, A (ac.) | CN*A | | | |
| CN ₁ | - | Impervious | 98 | 2.26 | 221.76 | | | |
| CN ₂ | В | Managed Turf | 61 | 0.47 | 28.64 | | | |
| CN ₃ | С | Managed Turf | 74 | 0.75 | 55.57 | | | |
| CN ₄ | D | Managed Turf | 80 | 2.35 | 188.06 | | | |
| CN ₅ | В | Brush (Good) | 48 | 2.59 | 124.15 | Includes adjacent 400 runoff | | |
| CN ₆ | С | Brush (Good) | 65 | 3.37 | 219.10 | includes adjacent 400 runon | | |
| CN ₇ | D | Brush (Good) | 73 | 2.27 | 165.87 | | | |
| CN ₈ | | | | | 0.00 | | | |
| CN ₉ | | | | | 0.00 | | | |
| CN ₁₀ | | | | | 0.00 | | | |
| | | | 14.06 | 1003.15 | | | | |
| Composite CN = | | | | | 71 | | | |

| Drainage Area: | Offsite Village area to Ex TOB Pond |
|----------------|-------------------------------------|
| | PREDEVELOPMENT |

| Time of Concentration, T _c | | | | | | | | |
|---------------------------------------|---------------|------------|--------------|---------------|-----------------------------|-----------------------------|--|--|
| 2 yr. Precip. (in.) = 2.73 | | | | | | | | |
| | | | | Roughness | | Travel Time, T _t | | |
| Flow Segment | Flow Regime | Land Cover | Length (ft) | Coeff., n | Slope (ft/ft) | (min.) | | |
| 1 | Sheet Flow | Grass | 100 | 0.24 | 0.07 | 9.4 | | |
| 2 | Shallow Conc. | Unpaved | 40 | | 0.35 | 0.1 | | |
| 3 | Channel | Grass | 1234 | 0.03 | 0.032 | 4.3 | | |
| 4 | | | | | | | | |
| 5 | | | | | | | | |
| 6 | | | | | | | | |
| 7 | | | | | | | | |
| 8 | | | | | | | | |
| 9 | | | | | | | | |
| 10 | | | | | | | | |
| | | | Total Time o | f Concentrati | on, T _c (min.) = | 13.7 | | |

| Runoff | | | | | | |
|--|-------|--------|---------|--|--|--|
| | 1 Yr. | 10 Yr. | 100 Yr. | | | |
| Precipitation (in.), P | 2.26 | 4.06 | 6.44 | | | |
| Composite CN | 71 | 71 | 71 | | | |
| Storage (in.) S=1000/CN-10 | 4.08 | 4.08 | 4.08 | | | |
| Initial abstraction (in.), I _a =0.2S | 0.82 | 0.82 | 0.82 | | | |
| Runoff depth (in.), Q=(P-0.2S) ² /[(P-I _a)+S] | 0.38 | 1.44 | 3.26 | | | |
| Runoff volume (ac-ft), RV = Q/12*A | 0.44 | 1.68 | 3.82 | | | |
| Flow rate (cfs), q _{peak} from hydrograph | 5.15 | 24.66 | | | | |
| | 0 | | | | | |

Hydrograph Number: 8

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 8

Offsite Village Area to Ex TOB Pond

| Hydrograph type | = SCS Runoff | Peak discharge | = 5.148 cfs |
|-----------------|--------------|--------------------|---------------|
| Storm frequency | = 1 yrs | Time to peak | = 724 min |
| Time interval | = 2 min | Hyd. volume | = 18,745 cuft |
| Drainage area | = 14.060 ac | Curve number | = 71 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 13.70 min |
| Total precip. | = 2.26 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 8

Offsite Village Area to Ex TOB Pond

| Hydrograph type | = SCS Runoff | Peak discharge | = 24.66 cfs |
|-----------------|--------------|--------------------|---------------|
| Storm frequency | = 10 yrs | Time to peak | = 724 min |
| Time interval | = 2 min | Hyd. volume | = 71,426 cuft |
| Drainage area | = 14.060 ac | Curve number | = 71 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 13.70 min |
| Total precip. | = 4.06 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



Drainage Area Runoff and Time of Concentration

Drainage Area: Onsite flow into Ex. TOB Pond

| | PREDEVELOPME | ENT | | | | |
|-----------------------------|-----------------|-------------------|-------|---------------|--------|--|
| Composite Curve Number (CN) | | | | | Notes: | |
| | Hydrologic Soil | | | | | |
| | Group | Land Cover | CN | Area, A (ac.) | CN*A | |
| CN ₁ | - | Impervious | 98 | 0.00 | 0.00 | |
| CN ₂ | В | Open Space (Good) | 61 | 3.64 | 221.94 | |
| CN ₃ | С | Open Space (Good) | 74 | 1.04 | 77.04 | |
| CN ₄ | | | | | 0.00 | |
| CN ₅ | | | | | 0.00 | |
| CN ₆ | | | | | 0.00 | |
| CN ₇ | | | | | 0.00 | |
| CN ₈ | | | | | 0.00 | |
| CN ₉ | | | | | 0.00 | |
| CN ₁₀ | | | | | 0.00 | |
| | · | | Total | 4.68 | 298.98 | |
| | | | Со | mposite CN = | 64 | |

| Time of Concentration, T _c | | | | | | |
|--|---------------|------------|-------------|-----------|---------------|-----------------------------|
| 2 yr. Precip. (in.) = 2.73 | | | | | | |
| | | | | Roughness | | Travel Time, T _t |
| Flow Segment | Flow Regime | Land Cover | Length (ft) | Coeff., n | Slope (ft/ft) | (min.) |
| 1 | Sheet Flow | Grass | 100 | 0.24 | 0.05 | 10.7 |
| 2 | Shallow Conc. | Unpaved | 380 | | 0.105 | 1.2 |
| 3 | Channel | Grass | 240 | 0.03 | 0.021 | 1.2 |
| 4 | | | | | | |
| 5 | | | | | | |
| 6 | | | | | | |
| 7 | | | | | | |
| 8 | | | | | | |
| 9 | | | | | | |
| 10 | | | | | | |
| Total Time of Concentration, T _c (min.) = | | | | | 13.2 | |

| Runoff | | | | |
|--|-------|--------|---------|--|
| | 1 Yr. | 10 Yr. | 100 Yr. | |
| Precipitation (in.), P | 2.26 | 4.06 | 6.44 | |
| Composite CN | 64 | 64 | 64 | |
| Storage (in.) S=1000/CN-10 | 5.63 | 5.63 | 5.63 | |
| Initial abstraction (in.), I _a =0.2S | 1.13 | 1.13 | 1.13 | |
| Runoff depth (in.), Q=(P-0.2S) ² /[(P-I _a)+S] | 0.19 | 1.01 | 2.58 | |
| Runoff volume (ac-ft), RV = Q/12*A | 0.07 | 0.39 | 1.01 | |
| Flow rate (cfs), q _{peak} from hydrograph | 0.56 | 6.28 | | |

Hydrograph Number: 9

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 9

Predev Onsite To TOB Pond

| Hydrograph type | = SCS Runoff | Peak discharge | = 0.559 cfs |
|-----------------|--------------|--------------------|--------------|
| Storm frequency | = 1 yrs | Time to peak | = 724 min |
| Time interval | = 2 min | Hyd. volume | = 3,334 cuft |
| Drainage area | = 4.680 ac | Curve number | = 64 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 13.20 min |
| Total precip. | = 2.26 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



Tuesday, 11 / 1 / 2022

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 9

Predev Onsite To TOB Pond

| Hydrograph type | = SCS Runoff | Peak discharge | = 6.280 cfs |
|-----------------|--------------|--------------------|---------------|
| Storm frequency | = 10 yrs | Time to peak | = 722 min |
| Time interval | = 2 min | Hyd. volume | = 17,630 cuft |
| Drainage area | = 4.680 ac | Curve number | = 64 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 13.20 min |
| Total precip. | = 4.06 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 10

Predev Total To Ex TOB Pond

| Hydrograph type Storm frequency | = Combine = 1 vrs | Peak discharge Time to peak | = 63.37 cfs = 726 min |
|------------------------------------|----------------------|--------------------------------|--------------------------|
| Time interval | $= 2 \min$ | Hyd. volume | = 231,959 cuft |
| Inflow hyds. | = 7, 8, 9 | Contrib. drain. area | = 18.740 ac |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 10

Predev Total To Ex TOB Pond

| Hydrograph type Storm frequency | = Combine = 10 vrs | Peak discharge Time to peak | = 168.79 cfs = 726 min |
|------------------------------------|-----------------------|--------------------------------|---------------------------|
| Time interval | $= 2 \min$ | Hyd. volume | = 661,724 cuft |
| Inflow hyds. | = 7, 8, 9 | Contrib. drain. area | = 18.740 ac |


Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Pond No. 6 - Ex. TOB Pond A

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 2018.40 ft

Stage / Storage Table

| Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|----------------|--|--|--|
| 2018.40 | 00 | 0 | 0 |
| 2019.00 | 40 | 8 | 8 |
| 2020.00 | 600 | 265 | 273 |
| 2021.00 | 2,410 | 1,404 | 1,677 |
| 2022.00 | 5,600 | 3,894 | 5,571 |
| 2022.10 | 6,095 | 585 | 6,156 |
| 2022.20 | 6,590 | 634 | 6,790 |
| 2022.30 | 7,085 | 683 | 7,473 |
| 2022.40 | 7,580 | 733 | 8,206 |
| 2022.50 | 8,075 | 783 | 8,989 |
| 2022.60 | 8,570 | 832 | 9,821 |
| 2022.70 | 9,065 | 882 | 10,703 |
| 2022.80 | 9,560 | 931 | 11,634 |
| 2022.90 | 10,055 | 981 | 12,614 |
| 2023.00 | 10,550 | 1,030 | 13,644 |
| 2024.00 | 12,758 | 11,635 | 25,279 |
| 2026.00 | 26,128 | 38,092 | 63,371 |
| 2028.00 | 37,922 | 63,679 | 127,050 |
| 2030.00 | 56,606 | 93,897 | 220,947 |
| 2032.00 | 83,164 | 138,907 | 359,854 |
| 2034.00 | 102,699 | 185,501 | 545,355 |
| | Elevation (ft) 2018.40 2019.00 2020.00 2021.00 2022.00 2022.10 2022.20 2022.30 2022.40 2022.50 2022.60 2022.70 2022.80 2022.90 2022.90 2023.00 2024.00 2024.00 2024.00 2024.00 2028.00 2030.00 2032.00 2034.00 | Elevation (ft)Contour area (sqft)2018.40002019.00402020.006002021.002,4102022.005,6002022.106,0952022.206,5902022.307,0852022.407,5802022.508,0752022.608,5702022.809,5602022.9010,0552023.0010,5502024.0012,7582024.0026,1282023.0037,9222030.0056,6062032.0083,1642034.00102,699 | Elevation (ft)Contour area (sqft)Incr. Storage (cuft)2018.400002019.004082020.006002652021.002,4101,4042022.005,6003,8942022.106,0955852022.206,5906342022.307,0856832022.407,5807332022.508,0757832022.608,5708322022.709,0658822022.809,5609312022.9010,0559812023.0010,5501,0302024.0026,12838,0922028.0037,92263,6792030.0056,60693,8972032.0083,164138,9072034.00102,699185,501 |

Culvert / Orifice Structures

Weir Structures

| | [A] | [B] | [C] | [PrfRsr] | | [A] | [B] | [C] | [D] |
|-----------------|-----------|---------|------|----------|----------------|---------------|-----------|------|------|
| Rise (in) | = 21.00 | 1.70 | 0.00 | 0.00 | Crest Len (ft) | = 9.42 | 40.00 | 0.00 | 0.00 |
| Span (in) | = 21.00 | 1.70 | 0.00 | 0.00 | Crest El. (ft) | = 2022.70 | 2032.00 | 0.00 | 0.00 |
| No. Barrels | = 1 | 1 | 0 | 0 | Weir Coeff. | = 3.33 | 2.60 | 3.33 | 3.33 |
| Invert El. (ft) | = 2018.30 | 2018.50 | 0.00 | 0.00 | Weir Type | = 1 | Broad | | |
| Length (ft) | = 125.00 | 0.50 | 0.00 | 0.00 | Multi-Stage | = Yes | No | No | No |
| Slope (%) | = 1.00 | 1.00 | 0.00 | n/a | | | | | |
| N-Value | = .013 | .013 | .013 | n/a | | | | | |
| Orifice Coeff. | = 0.60 | 0.60 | 0.60 | 0.60 | Exfil.(in/hr) | = 0.000 (by) | Wet area) | | |
| Multi-Stage | = n/a | Yes | No | No | TW Elev. (ft) | = 0.00 | | | |

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

| olugo / | otorugo / i | Bioonai go i | abio | | | | | | | | | | |
|-------------|-----------------|-----------------|--------------|--------------|--------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
| 0.00 | 0 | 2018.40 | 0.00 | 0.00 | | | 0.00 | 0.00 | | | | | 0.000 |
| 0.06 | 1 | 2018.46 | 0.06 ic | 0.00 | | | 0.00 | 0.00 | | | | | 0.000 |
| 0.12 | 2 | 2018.52 | 0.06 ic | 0.00 ic | | | 0.00 | 0.00 | | | | | 0.001 |
| 0.18 | 2 | 2018.58 | 0.06 ic | 0.01 ic | | | 0.00 | 0.00 | | | | | 0.009 |
| 0.24 | 3 | 2018.64 | 0.06 ic | 0.02 ic | | | 0.00 | 0.00 | | | | | 0.020 |
| 0.30 | 4 | 2018.70 | 0.06 ic | 0.03 ic | | | 0.00 | 0.00 | | | | | 0.027 |
| 0.36 | 5 | 2018.76 | 0.06 ic | 0.03 ic | | | 0.00 | 0.00 | | | | | 0.033 |
| 0.42 | 6 | 2018.82 | 0.06 ic | 0.04 ic | | | 0.00 | 0.00 | | | | | 0.038 |
| 0.48 | 6 | 2018.88 | 0.06 ic | 0.04 ic | | | 0.00 | 0.00 | | | | | 0.042 |
| 0.54 | 7 | 2018.94 | 0.06 ic | 0.05 ic | | | 0.00 | 0.00 | | | | | 0.046 |
| 0.60 | 8 | 2019.00 | 0.06 ic | 0.05 ic | | | 0.00 | 0.00 | | | | | 0.050 |
| 0.70 | 34 | 2019.10 | 0.06 ic | 0.06 ic | | | 0.00 | 0.00 | | | | | 0.055 |
| 0.80 | 61 | 2019.20 | 0.06 ic | 0.06 ic | | | 0.00 | 0.00 | | | | | 0.060 |
| 0.90 | 87 | 2019.30 | 0.07 ic | 0.06 ic | | | 0.00 | 0.00 | | | | | 0.065 |
| 1.00 | 114 | 2019.40 | 0.08 ic | 0.07 ic | | | 0.00 | 0.00 | | | | | 0.069 |
| 1.10 | 140 | 2019.50 | 0.08 ic | 0.07 ic | | | 0.00 | 0.00 | | | | | 0.073 |
| 1.20 | 167 | 2019.60 | 0.08 ic | 0.08 ic | | | 0.00 | 0.00 | | | | | 0.077 |
| 1.30 | 193 | 2019.70 | 0.08 ic | 0.08 ic | | | 0.00 | 0.00 | | | | | 0.081 |
| 1.40 | 220 | 2019.80 | 0.08 ic | 0.08 ic | | | 0.00 | 0.00 | | | | | 0.084 |
| 1.50 | 246 | 2019.90 | 0.09 ic | 0.09 ic | | | 0.00 | 0.00 | | | | | 0.087 |
| 1.60 | 273 | 2020.00 | 0.09 ic | 0.09 ic | | | 0.00 | 0.00 | | | | | 0.091 |
| 1.70 | 413 | 2020.10 | 0.09 ic | 0.09 ic | | | 0.00 | 0.00 | | | | | 0.094 |
| | | | | | | | | | | | | | |

Ex. TOB Pond Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|--------------|-----------------|-----------------|--------------|--------------|--------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| 1.80 | 554 | 2020.20 | 0.10 ic | 0.10 ic | | | 0.00 | 0.00 | | | | | 0.097 |
| 1.90 | 694 | 2020.30 | 0.11 ic | 0.10 ic | | | 0.00 | 0.00 | | | | | 0.100 |
| 2.00 | 835 | 2020.40 | 0.11 ic | 0.10 ic | | | 0.00 | 0.00 | | | | | 0.103 |
| 2.10 | 975 | 2020.50 | 0.11 ic | 0.11 ic | | | 0.00 | 0.00 | | | | | 0.105 |
| 2.20 | 1,115 | 2020.60 | 0.11 ic | 0.11 ic | | | 0.00 | 0.00 | | | | | 0.108 |
| 2.30 | 1,256 | 2020.70 | 0.12 ic | 0.11 ic | | | 0.00 | 0.00 | | | | | 0.111 |
| 2.40 | 1,396 | 2020.80 | 0.12 IC | 0.11 IC | | | 0.00 | 0.00 | | | | | 0.113 |
| 2.50 | 1,537 | 2020.90 | 0.12 IC | 0.12 IC | | | 0.00 | 0.00 | | | | | 0.116 |
| 2.00 | 1,077 | 2021.00 | 0.1210 | 0.12 IC | | | 0.00 | 0.00 | | | | | 0.118 |
| 2.70 | 2,000 | 2021.10 | 0.1210 | 0.12 IC | | | 0.00 | 0.00 | | | | | 0.121 |
| 2.00 | 2,430 | 2021.20 | 0.13 ic | 0.12 ic | | | 0.00 | 0.00 | | | | | 0.125 |
| 3.00 | 3 235 | 2021.00 | 0.13 ic | 0.13 ic | | | 0.00 | 0.00 | | | | | 0.120 |
| 3.10 | 3.624 | 2021.50 | 0.13 ic | 0.13 ic | | | 0.00 | 0.00 | | | | | 0.130 |
| 3.20 | 4,013 | 2021.60 | 0.13 ic | 0.13 ic | | | 0.00 | 0.00 | | | | | 0.132 |
| 3.30 | 4,403 | 2021.70 | 0.14 ic | 0.13 ic | | | 0.00 | 0.00 | | | | | 0.134 |
| 3.40 | 4,792 | 2021.80 | 0.14 ic | 0.14 ic | | | 0.00 | 0.00 | | | | | 0.136 |
| 3.50 | 5,182 | 2021.90 | 0.14 ic | 0.14 ic | | | 0.00 | 0.00 | | | | | 0.138 |
| 3.60 | 5,571 | 2022.00 | 0.14 ic | 0.14 ic | | | 0.00 | 0.00 | | | | | 0.141 |
| 3.61 | 5,630 | 2022.01 | 0.14 ic | 0.14 ic | | | 0.00 | 0.00 | | | | | 0.141 |
| 3.62 | 5,688 | 2022.02 | 0.14 ic | 0.14 ic | | | 0.00 | 0.00 | | | | | 0.141 |
| 3.63 | 5,747 | 2022.03 | 0.14 ic | 0.14 ic | | | 0.00 | 0.00 | | | | | 0.141 |
| 3.64 | 5,805 | 2022.04 | 0.14 ic | 0.14 ic | | | 0.00 | 0.00 | | | | | 0.141 |
| 3.65 | 5,863 | 2022.05 | 0.14 IC | 0.14 IC | | | 0.00 | 0.00 | | | | | 0.142 |
| 3.66 | 5,922 | 2022.06 | 0.14 IC | 0.14 IC | | | 0.00 | 0.00 | | | | | 0.142 |
| 3.07 | 5,980 | 2022.07 | 0.14 IC | 0.14 IC | | | 0.00 | 0.00 | | | | | 0.142 |
| 3.00 3.60 | 6,039 | 2022.00 | 0.14 IC | 0.14 IC | | | 0.00 | 0.00 | | | | | 0.142 |
| 3.09 | 6 156 | 2022.09 | 0.14 ic | 0.14 ic | | | 0.00 | 0.00 | | | | | 0.142 |
| 3.70 | 6 219 | 2022.10 | 0.14 ic | 0.14 ic | | | 0.00 | 0.00 | | | | | 0.143 |
| 3.72 | 6 283 | 2022.11 | 0.14 ic | 0.14 ic | | | 0.00 | 0.00 | | | | | 0.140 |
| 3.73 | 6.346 | 2022.13 | 0.14 ic | 0.14 ic | | | 0.00 | 0.00 | | | | | 0.143 |
| 3.74 | 6.409 | 2022.14 | 0.14 ic | 0.14 ic | | | 0.00 | 0.00 | | | | | 0.143 |
| 3.75 | 6,473 | 2022.15 | 0.14 ic | 0.14 ic | | | 0.00 | 0.00 | | | | | 0.144 |
| 3.76 | 6,536 | 2022.16 | 0.14 ic | 0.14 ic | | | 0.00 | 0.00 | | | | | 0.144 |
| 3.77 | 6,600 | 2022.17 | 0.14 ic | 0.14 ic | | | 0.00 | 0.00 | | | | | 0.144 |
| 3.78 | 6,663 | 2022.18 | 0.14 ic | 0.14 ic | | | 0.00 | 0.00 | | | | | 0.144 |
| 3.79 | 6,727 | 2022.19 | 0.14 ic | 0.14 ic | | | 0.00 | 0.00 | | | | | 0.144 |
| 3.80 | 6,790 | 2022.20 | 0.14 ic | 0.14 ic | | | 0.00 | 0.00 | | | | | 0.145 |
| 3.81 | 6,858 | 2022.21 | 0.14 ic | 0.14 ic | | | 0.00 | 0.00 | | | | | 0.145 |
| 3.82 | 6,927 | 2022.22 | 0.14 IC | 0.14 IC | | | 0.00 | 0.00 | | | | | 0.145 |
| 3.83 | 0,995 | 2022.23 | 0.15 IC | 0.15 IC | | | 0.00 | 0.00 | | | | | 0.145 |
| 3.04 | 7,003 | 2022.24 | 0.1510 | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.145 |
| 3.86 | 7,132 | 2022.23 | 0.15 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.140 |
| 3.87 | 7 268 | 2022.20 | 0.15 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.140 |
| 3.88 | 7 337 | 2022.21 | 0.15 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.146 |
| 3.89 | 7.405 | 2022.29 | 0.15 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.146 |
| 3.90 | 7,473 | 2022.30 | 0.15 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.147 |
| 3.91 | 7,547 | 2022.31 | 0.15 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.147 |
| 3.92 | 7,620 | 2022.32 | 0.15 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.147 |
| 3.93 | 7,693 | 2022.33 | 0.15 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.147 |
| 3.94 | 7,767 | 2022.34 | 0.15 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.147 |
| 3.95 | 7,840 | 2022.35 | 0.15 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.148 |
| 3.96 | 7,913 | 2022.36 | 0.15 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.148 |
| 3.97 | 7,986 | 2022.37 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.148 |
| 3.98 | 8,060 | 2022.38 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.148 |
| 3.99 | 8,133 | 2022.39 | 0.16 IC | 0.15 IC | | | 0.00 | 0.00 | | | | | 0.148 |
| 4.00 | 0,200 | 2022.40 | 0.101C | 0.15 IC | | | 0.00 | 0.00 | | | | | 0.140 |
| 4.01 | 0,200 | 2022.41 | 0.1010 | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.149 |
| 4.02 | 8 44 1 | 2022.42 | 0.10 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.149 |
| 4.03 | 8 519 | 2022.40 | 0 16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0 149 |
| 4.05 | 8 598 | 2022 45 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.149 |
| 4.06 | 8 676 | 2022 46 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.150 |
| 4.07 | 8,754 | 2022.47 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.150 |
| 4.08 | 8,832 | 2022.48 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.150 |
| 4.09 | 8,911 | 2022.49 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.150 |
| 4.10 | 8,989 | 2022.50 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.150 |
| 4.11 | 9,072 | 2022.51 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.151 |
| 4.12 | 9,155 | 2022.52 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.151 |
| 4.13 | 9,239 | 2022.53 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.151 |

Ex. TOB Pond Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|--------------|-----------------|-----------------|--------------|--------------|--------------|---------------|--------------------|-------------|-------------|-------------|--------------|-------------|--------------|
| 4.14 | 9,322 | 2022.54 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.151 |
| 4.15 | 9,405 | 2022.55 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.151 |
| 4.16 | 9,488 | 2022.56 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.152 |
| 4.17 | 9,571 | 2022.57 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.152 |
| 4.18 | 9,655 | 2022.58 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.152 |
| 4.19 | 9,738 | 2022.59 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.152 |
| 4.20 | 9,821 | 2022.60 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.152 |
| 4.21 | 9,909 | 2022.61 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.153 |
| 4.22 | 9,997 | 2022.62 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.153 |
| 4.23 | 10,085 | 2022.63 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.153 |
| 4.24 | 10,174 | 2022.64 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.153 |
| 4.25 | 10,262 | 2022.65 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.153 |
| 4.26 | 10,350 | 2022.66 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.153 |
| 4.27 | 10,438 | 2022.67 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.154 |
| 4.28 | 10,526 | 2022.68 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.154 |
| 4.29 | 10,614 | 2022.69 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.154 |
| 4.30 | 10,703 | 2022.70 | 0.16 ic | 0.15 ic | | | 0.00 | 0.00 | | | | | 0.154 |
| 4.31 | 10,796 | 2022.71 | 0.19 ic | 0.15 ic | | | 0.03 | 0.00 | | | | | 0.186 |
| 4.32 | 10,889 | 2022.72 | 0.25 ic | 0.15 ic | | | 0.09 | 0.00 | | | | | 0.244 |
| 4.33 | 10,982 | 2022.73 | 0.32 IC | 0.15 IC | | | 0.16 | 0.00 | | | | | 0.319 |
| 4.34 | 11,075 | 2022.74 | 0.43 ic | 0.15 IC | | | 0.25 | 0.00 | | | | | 0.407 |
| 4.35 | 11,168 | 2022.75 | 0.53 IC | 0.15 IC | | | 0.35 | 0.00 | | | | | 0.507 |
| 4.36 | 11,261 | 2022.76 | 0.64 IC | 0.15 IC | | | 0.46 | 0.00 | | | | | 0.617 |
| 4.37 | 11,354 | 2022.77 | 0.7610 | 0.15 IC | | | 0.58 | 0.00 | | | | | 0.737 |
| 4.38 | 11,447 | 2022.78 | 0.87 IC | 0.15 IC | | | 0.71 | 0.00 | | | | | 0.866 |
| 4.39 | 11,540 | 2022.79 | | 0.15 IC | | | 0.85 | 0.00 | | | | | 1.003 |
| 4.40 | 11,034 | 2022.80 | 1.18 IC | 0.15 IC | | | 0.99 | 0.00 | | | | | 1.140 |
| 4.41 | 11,732 | 2022.01 | 1.30 IC | 0.1510 | | | 1.10 | 0.00 | | | | | 1.290 |
| 4.42 | 11,030 | 2022.02 | 1.49 IC | 0.15 IC | | | 1.31 | 0.00 | | | | | 1.400 |
| 4.43 | 12,920 | 2022.03 | 1.03 10 | 0.1510 | | | 1.47 | 0.00 | | | | | 1.024 |
| 4.44 | 12,020 | 2022.04 | 2.01 ic | 0.1510 | | | 1.00 | 0.00 | | | | | 1.797 |
| 4.45 | 12,124 | 2022.03 | 2.01 IC | 0.15 ic | | | 2.01 | 0.00 | | | | | 2 161 |
| 4.40 | 12,222 | 2022.00 | 2.17 IC | 0.15 ic | | | 2.01 | 0.00 | | | | | 2.101 |
| 4.48 | 12,020 | 2022.07 | 2.00 lc | 0.15 ic | | | 2.20 | 0.00 | | | | | 2.502 |
| 4 4 9 | 12,410 | 2022.80 | 2.01 ic | 0.15 ic | | | 2.40 | 0.00 | | | | | 2 751 |
| 4.50 | 12.614 | 2022.90 | 2.99 ic | 0.15 ic | | | 2.81 | 0.00 | | | | | 2.956 |
| 4.51 | 12,717 | 2022.91 | 3.18 ic | 0.15 ic | | | 3.02 | 0.00 | | | | | 3.169 |
| 4.52 | 12,820 | 2022.92 | 3.39 ic | 0.15 ic | | | 3.24 | 0.00 | | | | | 3.387 |
| 4.53 | 12,923 | 2022.93 | 3.61 ic | 0.15 ic | | | 3.46 | 0.00 | | | | | 3.610 |
| 4.54 | 13,026 | 2022.94 | 3.91 ic | 0.15 ic | | | 3.69 | 0.00 | | | | | 3.838 |
| 4.55 | 13,129 | 2022.95 | 4.12 ic | 0.15 ic | | | 3.92 | 0.00 | | | | | 4.071 |
| 4.56 | 13,232 | 2022.96 | 4.34 ic | 0.15 ic | | | 4.16 | 0.00 | | | | | 4.308 |
| 4.57 | 13,335 | 2022.97 | 4.57 ic | 0.15 ic | | | 4.40 | 0.00 | | | | | 4.551 |
| 4.58 | 13,438 | 2022.98 | 4.80 ic | 0.15 ic | | | 4.65 | 0.00 | | | | | 4.797 |
| 4.59 | 13,541 | 2022.99 | 5.05 ic | 0.15 ic | | | 4.90 | 0.00 | | | | | 5.048 |
| 4.60 | 13,644 | 2023.00 | 5.36 ic | 0.14 ic | | | 5.16 | 0.00 | | | | | 5.301 |
| 4.70 | 14,808 | 2023.10 | 8.09 ic | 0.14 ic | | | 7.94 | 0.00 | | | | | 8.077 |
| 4.80 | 15,971 | 2023.20 | 11.22 ic | 0.13 ic | | | 11.09 | 0.00 | | | | | 11.22 |
| 4.90 | 17,135 | 2023.30 | 14.70 ic | 0.12 ic | | | 14.58 | 0.00 | | | | | 14.70 |
| 5.00 | 18,298 | 2023.40 | 18.46 oc | 0.09 ic | | | 18.37 | 0.00 | | | | | 18.46 |
| 5.10 | 19,462 | 2023.50 | 21.38 oc | 0.06 ic | | | 21.32 s | 0.00 | | | | | 21.38 |
| 5.20 | 20,625 | 2023.60 | 22.11 oc | 0.05 IC | | | 22.06 s | 0.00 | | | | | 22.11 |
| 5.30 | 21,789 | 2023.70 | 22.63 oc | 0.04 IC | | | 22.58 s | 0.00 | | | | | 22.63 |
| 5.40 | 22,952 | 2023.80 | 23.04 oc | 0.04 IC | | | 23.00 s | 0.00 | | | | | 23.04 |
| 5.50 | 24,116 | 2023.90 | 23.40 oc | 0.03 IC | | | 23.36 S | 0.00 | | | | | 23.40 |
| 5.60 | 25,279 | 2024.00 | 23.72.00 | | | | 23.09 S | 0.00 | | | | | 23.72 |
| 0.00 6.00 | 29,000 | 2024.20 | 24.29 00 | 0.02 ic | | | 24.27 S | 0.00 | | | | | 24.29 |
| 6.20 | 32,090 | 2024.40 | 24.01.00 | 0.02 ic | | | 24.795 | 0.00 | | | | | 24.01 |
| 6.40 | 40 516 | 2024.00 | 25.30 00 | 0.02 ic | | | 25.275 | 0.00 | | | | | 25.29 |
| 6.60 | 40,310 | 2024.00 | 26.22 oc | 0.02 ic | | | 25.74 S 26 10 s | 0.00 | | | | | 26.20 |
| 6.80 | 48 134 | 2025 20 | 26 65 00 | 0.01 ic | | | 26.103 26.64 s | 0.00 | | | | | 26.65 |
| 7.00 | 51 944 | 2025 40 | 27.08 00 | 0.01 ic | | | 27 03 s | 0.00 | | | | | 27 05 |
| 7 20 | 55 753 | 2025 60 | 27 49 00 | 0.01 ic | | | 27 46 c | 0.00 | | | | | 27 47 |
| 7.40 | 59 562 | 2025 80 | 27.90 oc | 0.01 ic | | | 27.85 s | 0.00 | | | | | 27.86 |
| 7.60 | 63.371 | 2026.00 | 28.31 oc | 0.01 ic | | | 28.27 s | 0.00 | | | | | 28.28 |
| 7.80 | 69.739 | 2026.20 | 28.70 oc | 0.01 ic | | | 28.64 s | 0.00 | | | | | 28.65 |
| 8.00 | 76.107 | 2026.40 | 29.09 oc | 0.01 ic | | | 29.03 s | 0.00 | | | | | 29.04 |
| 8.20 | 82,475 | 2026.60 | 29.47 oc | 0.01 ic | | | 29.42 s | 0.00 | | | | | 29.42 |
| 8.40 | 88,843 | 2026.80 | 29.85 oc | 0.01 ic | | | 29.80 s | 0.00 | | | | | 29.81 |
| 8.60 | 95,210 | 2027.00 | 30.22 oc | 0.01 ic | | | 30.18 s | 0.00 | | | | | 30.19 |

Ex. TOB Pond Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| 8.80 | 101,578 | 2027.20 | 30.59 oc | 0.01 ic | | | 30.50 s | 0.00 | | | | | 30.51 |
| 9.00 | 107,946 | 2027.40 | 30.96 oc | 0.01 ic | | | 30.90 s | 0.00 | | | | | 30.91 |
| 9.20 | 114,314 | 2027.60 | 31.32 oc | 0.01 ic | | | 31.17 s | 0.00 | | | | | 31.18 |
| 9.40 | 120,682 | 2027.80 | 31.67 oc | 0.01 ic | | | 31.62 s | 0.00 | | | | | 31.63 |
| 9.60 | 127,050 | 2028.00 | 32.02 oc | 0.01 ic | | | 31.96 s | 0.00 | | | | | 31.97 |
| 9.80 | 136,440 | 2028.20 | 32.37 oc | 0.01 ic | | | 32.19 s | 0.00 | | | | | 32.19 |
| 10.00 | 145,829 | 2028.40 | 32.71 oc | 0.01 ic | | | 32.46 s | 0.00 | | | | | 32.47 |
| 10.20 | 155,219 | 2028.60 | 33.05 oc | 0.01 ic | | | 32.96 s | 0.00 | | | | | 32.96 |
| 10.40 | 164,609 | 2028.80 | 33.39 oc | 0.00 ic | | | 33.30 s | 0.00 | | | | | 33.30 |
| 10.60 | 173,998 | 2029.00 | 33.72 oc | 0.00 ic | | | 33.53 s | 0.00 | | | | | 33.53 |
| 10.80 | 183,388 | 2029.20 | 34.05 oc | 0.00 ic | | | 34.01 s | 0.00 | | | | | 34.01 |
| 11.00 | 192,778 | 2029.40 | 34.38 oc | 0.00 ic | | | 34.12 s | 0.00 | | | | | 34.13 |
| 11.20 | 202,167 | 2029.60 | 34.70 oc | 0.00 ic | | | 34.44 s | 0.00 | | | | | 34.44 |
| 11.40 | 211,557 | 2029.80 | 35.02 oc | 0.00 ic | | | 34.67 s | 0.00 | | | | | 34.68 |
| 11.60 | 220,947 | 2030.00 | 35.34 oc | 0.00 ic | | | 34.87 s | 0.00 | | | | | 34.88 |
| 11.80 | 234,838 | 2030.20 | 35.65 oc | 0.00 ic | | | 35.43 s | 0.00 | | | | | 35.44 |
| 12.00 | 248,728 | 2030.40 | 35.96 oc | 0.00 ic | | | 35.96 s | 0.00 | | | | | 35.96 |
| 12.20 | 262,619 | 2030.60 | 36.27 oc | 0.00 ic | | | 35.86 s | 0.00 | | | | | 35.87 |
| 12.40 | 276,510 | 2030.80 | 36.58 oc | 0.00 ic | | | 36.27 s | 0.00 | | | | | 36.27 |
| 12.60 | 290,400 | 2031.00 | 36.88 oc | 0.00 ic | | | 36.63 s | 0.00 | | | | | 36.63 |
| 12.80 | 304,291 | 2031.20 | 37.18 oc | 0.00 ic | | | 37.10 s | 0.00 | | | | | 37.10 |
| 13.00 | 318,182 | 2031.40 | 37.48 oc | 0.00 ic | | | 37.37 s | 0.00 | | | | | 37.37 |
| 13.20 | 332,073 | 2031.60 | 37.78 oc | 0.00 ic | | | 37.57 s | 0.00 | | | | | 37.58 |
| 13.40 | 345,963 | 2031.80 | 38.07 oc | 0.00 ic | | | 37.73 s | 0.00 | | | | | 37.73 |
| 13.60 | 359,854 | 2032.00 | 38.37 oc | 0.00 ic | | | 37.71 s | 0.00 | | | | | 37.71 |
| 13.80 | 378,404 | 2032.20 | 38.66 oc | 0.00 ic | | | 38.61 s | 9.30 | | | | | 47.91 |
| 14.00 | 396,954 | 2032.40 | 38.94 oc | 0.00 ic | | | 38.82 s | 26.30 | | | | | 65.12 |
| 14.20 | 415,504 | 2032.60 | 39.23 oc | 0.00 ic | | | 38.74 s | 48.32 | | | | | 87.06 |
| 14.40 | 434,055 | 2032.80 | 39.51 oc | 0.00 ic | | | 38.58 s | 74.39 | | | | | 112.97 |
| 14.60 | 452,605 | 2033.00 | 39.79 oc | 0.00 ic | | | 39.43 s | 103.96 | | | | | 143.40 |
| 14.80 | 471,155 | 2033.20 | 40.07 oc | 0.00 ic | | | 39.17 s | 136.66 | | | | | 175.83 |
| 15.00 | 489,705 | 2033.40 | 40.35 oc | 0.00 ic | | | 40.00 s | 172.21 | | | | | 212.22 |
| 15.20 | 508,255 | 2033.60 | 40.63 oc | 0.00 ic | | | 39.60 s | 210.40 | | | | | 250.01 |
| 15.40 | 526,805 | 2033.80 | 40.90 oc | 0.00 ic | | | 40.42 s | 251.06 | | | | | 291.49 |
| 15.60 | 545.355 | 2034.00 | 41.17 oc | 0.00 ic | | | 41.07 s | 294.16 | | | | | 335.23 |

...End

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 11

Predev Ex.TOB Pond Out

| Hydrograph type | = Reservoir | Peak discharge | = 27.06 cfs |
|-----------------|--------------------------|-------------------------------|----------------|
| Storm frequency | = 1 yrs | Time to peak | = 740 min |
| Time interval | = 2 min | Hyd. volume | = 231,958 cuft |
| Inflow hyd. No. | = 10 - Predev Total To E | x TOB Roa d. Elevation | = 2025.41 ft |
| Reservoir name | = Ex. TOB Pond | Max. Storage | = 52,034 cuft |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 11

Predev Ex.TOB Pond Out

| Hydrograph type | = Reservoir | Peak discharge | = 35.75 cfs |
|-----------------|--------------------------|--------------------------------|----------------|
| Storm frequency | = 10 yrs | Time to peak | = 752 min |
| Time interval | = 2 min | Hyd. volume | = 661,723 cuft |
| Inflow hyd. No. | = 10 - Predev Total To E | x TOB Rolax . Elevation | = 2030.32 ft |
| Reservoir name | = Ex. TOB Pond | Max. Storage | = 243,216 cuft |





Drainage Area Runoff and Time of Concentration

Drainage Area: To 460 south culvert crossing (excludes Union area) PREDEVELOPMENT

| | C | | Notes: | | | |
|------------------|-----------------|--------------|--------|---------------|---------|--|
| | Hydrologic Soil | | | | | |
| | Group | Land Cover | CN | Area, A (ac.) | CN*A | |
| CN ₁ | - | Impervious | 98 | 14.92 | 1461.92 | |
| CN ₂ | В | Managed Turf | 61 | 0.53 | 32.46 | |
| CN ₃ | C | Managed Turf | 74 | 5.55 | 410.68 | |
| CN_4 | В | Brush (Good) | 48 | 0.72 | 34.62 | |
| CN ₅ | С | Brush (Good) | 65 | 1.66 | 107.68 | |
| CN ₆ | | | | | 0.00 | |
| CN ₇ | | | | | 0.00 | |
| CN ₈ | | | | | 0.00 | |
| CN ₉ | | | | | 0.00 | |
| CN ₁₀ | | | | | 0.00 | |
| | | 2047.36 | | | | |
| Composite CN = | | | | | 88 | |

| | Time of Concentration, T _c | | | | | | | | | |
|--|---------------------------------------|-----------------------|-------------|-----------|---------------|-----------------------------|--|--|--|--|
| | | 2 yr. Precip. (in.) = | 2.73 | | | | | | | |
| | | | | Roughness | | Travel Time, T _t | | | | |
| Flow Segment | Flow Regime | Land Cover | Length (ft) | Coeff., n | Slope (ft/ft) | (min.) | | | | |
| 1 | Sheet Flow | Paved | 100 | 0.011 | 0.030 | 1.1 | | | | |
| 2 | Shallow Conc. | Paved | 131 | | 0.023 | 0.7 | | | | |
| 3 | Channel | Curb | 101 | 0.011 | 0.005 | 0.4 | | | | |
| 4 | Channel | Pipe 30" | 394 | 0.011 | 0.010 | 0.9 | | | | |
| 5 | Channel | Grass | 865 | 0.03 | 0.044 | 3.1 | | | | |
| 6 | | | | | | | | | | |
| 7 | | | | | | | | | | |
| 8 | | | | | | | | | | |
| 9 | | | | | | | | | | |
| 10 | | | | | | | | | | |
| Total Time of Concentration, T _c (min.) = | | | | | | | | | | |

| Runoff | | | |
|--|-------|--------|---------|
| | 1 Yr. | 10 Yr. | 100 Yr. |
| Precipitation (in.), P | 2.26 | 4.06 | 6.44 |
| Composite CN | 88 | 88 | 88 |
| Storage (in.) S=1000/CN-10 | 1.36 | 1.36 | 1.36 |
| Initial abstraction (in.), $I_a=0.2S$ | 0.27 | 0.27 | 0.27 |
| Runoff depth (in.), Q=(P-0.2S) ² /[(P-I _a)+S] | 1.18 | 2.78 | 5.05 |
| Runoff volume (ac-ft), RV = Q/12*A | 2.30 | 5.42 | 9.84 |
| Flow rate (cfs), q _{peak} from hydrograph | 46.38 | 106.50 | |
| Libratura ana la Niversia an | 10 | | |

Hydrograph Number: 13

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 13

To 460 South Culvert (excluding Union)

| Hydrograph type = | SCS Runoff | Peak discharge | = 46.38 cfs |
|-------------------|-------------|--------------------|---------------|
| Storm frequency = | = 1 yrs | Time to peak | = 716 min |
| Time interval = | = 2 min | Hyd. volume | = 93,772 cuft |
| Drainage area = | = 23.380 ac | Curve number | = 88 |
| Basin Slope = | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method = | = User | Time of conc. (Tc) | = 6.20 min |
| Total precip. = | = 2.26 in | Distribution | = Type II |
| Storm duration = | = 24 hrs | Shape factor | = 484 |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Friday, 04 / 29 / 2022

Hyd. No. 13

To 460 South Culvert (excluding Union)

| Hydrograph type | = SCS Runoff | Peak discharge | = 106.50 cfs |
|-----------------|--------------|--------------------|----------------|
| Storm frequency | = 10 yrs | Time to peak | = 716 min |
| Time interval | = 2 min | Hyd. volume | = 221,560 cuft |
| Drainage area | = 23.380 ac | Curve number | = 88 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 6.20 min |
| Total precip. | = 4.06 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



WORKSHEET FOR SCS HYDROLOGIC PARAMETERS

| | Existing | Project: Sturbridge Apartments |
|--------------------|------------|--|
| Site Conditions: | X Proposed | Subarea Number: 2b - No Detention - Bypass |
| | Existing | By: Justin Brown |
| Off-Site Land Use: | X Proposed | Date: 4/13/2020 |

RUNOFF CURVE NUMBER

| Soil Group | Land Use or Zoning | | Area (acres) | RCN | RCN x Area | |
|---------------|--------------------|------------|-----------------|-----|---------------|--|
| В | On-Site | Impervious | 0.43 | 98 | 42.14 | |
| В | On-Site | Open Space | 1.14 | 61 | 69.54 | |
| С | On-Site | Impervious | 0.00 | 98 | 0 | |
| С | On-Site | Open Space | 0.08 | 74 | 5.92 | |
| | | | | | | |
| | | | | | | |
| | | | | | <u></u> | |
| | | | | | | |
| | | | | | - | |
| | | | | | | |
| | | | | | | |

Total Area

0.003 sq. mi

Weighted RCN =

71

Notes:

1.65

ac

Time of Concentration = 18.39 minutes (See Attached)

| TR 55 Worksheet: Time of Concentration (Tc) | PROJECT | PROJECT: TNHSE19001 | | | PN: (Post-DEVELOPMENT: POI#2 | | | |
|---|-------------|---------------------|----------|----------|------------------------------|----------|----------|---|
| | 1 | 2 | 3 | 4 | 5 | 6 | 6 | |
| Sheet Flow | | | | | | | | |
| Surface description (Table 3-1) | Dense Grass | | | | | | | |
| Manning's roughness coeff., n (Table 3-1) | 0.24 | | | | | 1 | | |
| Flow length, L (total L < 100 ft) ft | 100.00 | | | | | | | |
| Two-year 24-hour rainfall, P2 in | 2.74 | | | | | | | |
| Land slope, S ft/ft | 0.0300 | | | | | | | |
| $T_t = (0.007 (nL)^{0.8}) / (P_2^{0.5} s^{0.4}) \dots hr$ | 0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Shallow Concetrated Flow | | | | | | | | |
| Surface description (paved=1 or unpaved=0) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Flow length, L ft | 223.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Watercourse slope, S ft/ft | 0.0540 | 0.0100 | 0.0100 | 0.0100 | 0.0100 | 0.0100 | 0.0100 | |
| Average velocity, V ft/s | - | | - | | - | | | |
| Unpaved V = $16.1345 (s)^{0.5}$ | 3.75 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 | |
| Paved $V = 20.3282 (s)^{0.5}$ | | | | | | | | |
| T _t = L /3600Vhr | 0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Channel Flow | CHANNEL | | | | | | 3 | |
| Cross sectional flow area, A ft ² | 3.00 | 1.20 | 3.10 | | | | | |
| Wetted perimeter, Pw ft | 6.00 | 4.00 | 6.28 | 0 | | | | |
| Hydraulic radius, r = A/Pwft | 0.50 | 0.30 | 0.49 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Channel slope, s ft/ft | 0.050 | 0.033 | 0.010 | 1 | | i | | |
| Manning's roughness coefficient, n | 0.011 | 0.035 | 0.069 | 0.013 | 0.013 | 0.013 | 0.013 | |
| Velocity, V=(1.49/n)R ^{2/3} s ^{1/2} ft | 19.08 | 3.47 | 1.35 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Flow length, L ft | 227.0 | 223.0 | 244.0 | | | | | |
| T _t = L/3600Vhr | 0.003 | 0.018 | 0.050 | 0.000 | 0.000 | 0.000 | 0.000 | |
| Sub Basin Tc = $T_{sheetflow} + T_{shallow concentrated} + T_{channel} =$ | 0.24 hr | 0.02 hr | 0.05 hr | 0.00 hr | 0.00 hr | 0.00 hr | 0.00 hr | |
| Sub Basin Tc = $T_{sheetflow} + T_{shallow concentrated} + T_{channel} =$ | 14.30 min | 1.07 min | 3.02 min | 0.00 min | 0.00 min | 0.00 min | 0.00 min | 1 |

18.39 min

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 14

Union Bypass To 460 S Culvert

| Hydrograph type | = SCS Runoff | Peak discharge | = 0.535 cfs |
|-----------------|--------------|--------------------|--------------|
| Storm frequency | = 1 yrs | Time to peak | = 726 min |
| Time interval | = 2 min | Hyd. volume | = 2,256 cuft |
| Drainage area | = 1.650 ac | Curve number | = 71 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 18.40 min |
| Total precip. | = 2.26 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 14

Union Bypass To 460 S Culvert

| Hydrograph type | = SCS Runoff | Peak discharge | = 2.647 cfs |
|-----------------|--------------|--------------------|--------------|
| Storm frequency | = 10 yrs | Time to peak | = 726 min |
| Time interval | = 2 min | Hyd. volume | = 8,597 cuft |
| Drainage area | = 1.650 ac | Curve number | = 71 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 18.40 min |
| Total precip. | = 4.06 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



WORKSHEET FOR SCS HYDROLOGIC PARAMETERS

| | 1.00 | Existing | Project: | Sturbridge Apartments | | | |
|--------------------|------|----------|------------------------------|-----------------------|--|--|--|
| Site Conditions: | X | Proposed | Subarea Number: 2a Detention | | | | |
| | | Existing | By: | Justin Brown | | | |
| Off-Site Land Use: | X | Proposed | Date: | 4/13/2020 | | | |

RUNOFF CURVE NUMBER

| Soil Group | Land Use or Zoning | | Area (acres) | RCN | RCN x Area |
|---------------|--------------------|------------|-----------------|-----|---------------|
| В | On-Site | Impervious | 2.12 | 98 | 207.76 |
| В | On-Site | Open Space | 0.13 | 61 | 7.93 |
| С | On-Site | Impervious | 1.31 | 98 | 128.38 |
| С | On-Site Open Space | Open Space | 0.16 | 74 | 11.84 |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | - | | | | |

Total Area

0.006 sq. mi

Weighted RCN =

96

Notes:

3.72

ac

Time of Concentration = 5 minutes (Assumed)

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 15

Union South Basin Inflow

| Hydrograph type | = SCS Runoff | Peak discharge | = 10.62 cfs |
|-----------------|--------------|--------------------|---------------|
| Storm frequency | = 1 yrs | Time to peak | = 716 min |
| Time interval | = 2 min | Hyd. volume | = 23,128 cuft |
| Drainage area | = 3.720 ac | Curve number | = 96 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 5.00 min |
| Total precip. | = 2.26 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



Friday, 04 / 29 / 2022

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 15

Union South Basin Inflow

| Hydrograph type | = SCS Runoff | Peak discharge | = 20.05 cfs |
|-----------------|--------------|--------------------|---------------|
| Storm frequency | = 10 yrs | Time to peak | = 716 min |
| Time interval | = 2 min | Hyd. volume | = 45,569 cuft |
| Drainage area | = 3.720 ac | Curve number | = 96 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 5.00 min |
| Total precip. | = 4.06 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Pond No. 11 - Union South Underground Det.

Pond Data

UG Chambers -Invert elev. = 2052.00 ft, Rise x Span = 4.00×4.00 ft, Barrel Len = 140.00 ft, No. Barrels = 4, Slope = 0.50%, Headers = Yes **Encasement -**Invert elev. = 2051.50 ft, Width = 6.50 ft, Height = 5.50 ft, Voids = 40.00%

Stage / Storage Table

| Stage (ft) Elevation (ft) | | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|---------------------------|---------|---------------------|----------------------|----------------------|
| 0.00 | 2051.50 | n/a | 0 | 0 |
| 0.62 | 2052.12 | n/a | 462 | 462 |
| 1.24 | 2052.74 | n/a | 1,212 | 1,674 |
| 1.86 | 2053.36 | n/a | 1,655 | 3,329 |
| 2.48 | 2053.98 | n/a | 1,832 | 5,161 |
| 3.10 | 2054.60 | n/a | 1,888 | 7,049 |
| 3.72 | 2055.22 | n/a | 1,850 | 8,899 |
| 4.34 | 2055.84 | n/a | 1,703 | 10,602 |
| 4.96 | 2056.46 | n/a | 1,328 | 11,930 |
| 5.58 | 2057.08 | n/a | 1,009 | 12,939 |
| 6.20 | 2057.70 | n/a | 987 | 13,925 |

Culvert / Orifice Structures

Weir Structures

| | [A] | [B] | [C] | [PrfRsr] | | [A] | [B] | [C] | [D] |
|-----------------|-----------|---------|---------|----------|----------------|-------------|-----------|------|------|
| Rise (in) | = 24.00 | 8.50 | 4.88 | 0.00 | Crest Len (ft) | = 18.85 | 0.73 | 0.00 | 0.00 |
| Span (in) | = 24.00 | 7.00 | 72.00 | 0.00 | Crest El. (ft) | = 2058.71 | 2056.10 | 0.00 | 0.00 |
| No. Barrels | = 1 | 1 | 1 | 0 | Weir Coeff. | = 3.33 | 3.33 | 3.33 | 3.33 |
| Invert El. (ft) | = 2051.50 | 2051.50 | 2054.55 | 0.00 | Weir Type | = 1 | Rect | | |
| Length (ft) | = 25.00 | 0.50 | 0.50 | 0.00 | Multi-Stage | = Yes | Yes | No | No |
| Slope (%) | = 1.00 | 0.00 | 0.00 | n/a | | | | | |
| N-Value | = .013 | .013 | .013 | n/a | | | | | |
| Orifice Coeff. | = 0.60 | 0.60 | 0.60 | 0.60 | Exfil.(in/hr) | = 0.000 (by | Wet area) | | |
| Multi-Stage | = n/a | Yes | Yes | No | TW Elev. (ft) | = 0.00 | | | |

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s). Stage / Storage / Discharge Table

| - | | | · | | | | | | | | | | |
|-------------|-----------------|-----------------|--------------|--------------|--------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| Stage ft | Storage cuft | Elevation ft | CIV A cfs | CIV B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | rotal cfs |
| 0.00 | 0 | 2051.50 | 0.00 | 0.00 | 0.00 | | 0.00 | 0.00 | | | | | 0.000 |
| 0.06 | 46 | 2051.56 | 0.02 ic | 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.018 |
| 0.12 | 92 | 2051.62 | 0.06 ic | 0.06 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.059 |
| 0.19 | 139 | 2051.69 | 0.12 ic | 0.12 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.119 |
| 0.25 | 185 | 2051.75 | 0.20 ic | 0.19 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.191 |
| 0.31 | 231 | 2051.81 | 0.29 ic | 0.28 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.276 |
| 0.37 | 277 | 2051.87 | 0.38 ic | 0.38 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.378 |
| 0.43 | 324 | 2051.93 | 0.48 ic | 0.48 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.483 |
| 0.50 | 370 | 2052.00 | 0.60 ic | 0.60 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.602 |
| 0.56 | 416 | 2052.06 | 0.73 ic | 0.73 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.734 |
| 0.62 | 462 | 2052.12 | 0.89 ic | 0.86 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.863 |
| 0.68 | 584 | 2052.18 | 1.01 ic | 1.01 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.010 |
| 0.74 | 705 | 2052.24 | 1.13 ic | 1.12 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.124 |
| 0.81 | 826 | 2052.31 | 1.20 ic | 1.20 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.201 |
| 0.87 | 947 | 2052.37 | 1.27 ic | 1.27 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.274 |
| 0.93 | 1,068 | 2052.43 | 1.35 ic | 1.35 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.346 |
| 0.99 | 1,189 | 2052.49 | 1.42 ic | 1.42 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.418 |
| 1.05 | 1,311 | 2052.55 | 1.49 ic | 1.49 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.489 |
| 1.12 | 1,432 | 2052.62 | 1.56 ic | 1.56 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.556 |
| 1.18 | 1,553 | 2052.68 | 1.64 ic | 1.62 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.616 |
| 1.24 | 1,674 | 2052.74 | 1.73 ic | 1.67 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.674 |
| 1.30 | 1,840 | 2052.80 | 1.74 ic | 1.74 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.738 |
| 1.36 | 2,005 | 2052.86 | 1.81 ic | 1.80 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.799 |
| 1.43 | 2,171 | 2052.93 | 1.90 ic | 1.85 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.851 |
| 1.49 | 2,336 | 2052.99 | 1.91 ic | 1.91 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.910 |
| 1.55 | 2,502 | 2053.05 | 1.99 ic | 1.97 ic | 0.00 | | 0.00 | 0.00 | | | | | 1.965 |
| 1.61 | 2.667 | 2053.11 | 2.01 ic | 2.01 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.014 |
| 1.67 | 2.833 | 2053.17 | 2.08 ic | 2.07 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.073 |
| 1.74 | 2,998 | 2053.24 | 2.18 ic | 2.12 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.118 |
| 1.80 | 3,164 | 2053.30 | 2.18 ic | 2.18 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.175 |
| 1.86 | 3.329 | 2053.36 | 2.28 ic | 2.22 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.218 |
| 1.92 | 3 513 | 2053 42 | 2 28 ic | 2 27 ic | 0.00 | | 0.00 | 0.00 | | | | | 2 273 |
| | 0,0.0 | | | | 0.00 | | 0.00 | 0.00 | | | | | 0 |

Union South Underground Det. Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| 1.98 | 3,696 | 2053.48 | 2.38 ic | 2.31 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.313 |
| 2.05 | 3,879 | 2053.55 | 2.38 ic | 2.37 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.366 |
| 2.11 | 4,062 | 2053.61 | 2.41 ic | 2.41 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.405 |
| 2.17 | 4,245 | 2053.67 | 2.48 ic | 2.46 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.456 |
| 2.23 | 4,428 | 2053.73 | 2.50 ic | 2.50 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.498 |
| 2.29 | 4,612 | 2053.79 | 2.59 ic | 2.54 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.542 |
| 2.36 | 4,795 | 2053.86 | 2.59 ic | 2.59 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.589 |
| 2.42 | 4,978 | 2053.92 | 2.70 ic | 2.63 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.626 |
| 2.48 | 5,161 | 2053.98 | 2.70 ic | 2.67 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.672 |
| 2.54 | 5,350 | 2054.04 | 2.71 ic | 2.71 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.712 |
| 2.60 | 5,539 | 2054.10 | 2.81 ic | 2.75 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.752 |
| 2.67 | 5,728 | 2054.17 | 2.81 IC | 2.80 ic | 0.00 | | 0.00 | 0.00 | | | | | 2.796 |
| 2.73 | 5,916 | 2054.23 | 2.83 IC | 2.83 IC | 0.00 | | 0.00 | 0.00 | | | | | 2.831 |
| 2.79 | 6,105 | 2054.29 | 2.92 ic | 2.87 IC | 0.00 | | 0.00 | 0.00 | | | | | 2.8/2 |
| 2.85 | 6,294 | 2054.35 | 2.92 ic | 2.91 IC | 0.00 | | 0.00 | 0.00 | | | | | 2.915 |
| 2.91 | 6,483 | 2054.41 | 2.95 IC | 2.95 IC | 0.00 | | 0.00 | 0.00 | | | | | 2.947 |
| 2.98 | 6,672 | 2054.48 | 3.03 IC | 2.99 IC | 0.00 | | 0.00 | 0.00 | | | | | 2.988 |
| 3.04 | 0,800 | 2054.54 | 3.03 IC | 3.03 IC | 0.00 | | 0.00 | 0.00 | | | | | 3.028 |
| 3.10 | 7,049 | 2054.60 | 3.32 OC | 3.04 IC | 0.23 IC | | 0.00 | 0.00 | | | | | 3.208 |
| 3.10 | 7,234 | 2004.00 | 3.60 00 | 3.03 IC | | | 0.00 | 0.00 | | | | | 3.790 |
| 3.22 | 7,419 | 2054.72 | 4.49 OC | 3.00 IC | 1.48 IC | | 0.00 | 0.00 | | | | | 4.48Z |
| 3.29 | 7,604 | 2054.79 | 5.38 OC | 2.95 IC | 2.34 IC | | 0.00 | 0.00 | | | | | 5.289 |
| 3.35 | 7,789 | 2054.85 | 0.24 OC | 2.89 IC | 3.32 IC | | 0.00 | 0.00 | | | | | 0.210 |
| 3.41 | 7,974 | 2054.91 | 7.28 OC | 2.81 IC | 4.41 IC | | 0.00 | 0.00 | | | | | 1.221 |
| 3.47 | 8,159 | 2054.97 | 8.20 OC | 2.72 IC | 5.50 IC | | 0.00 | 0.00 | | | | | 0.21/ |
| 3.33 | 0,344 | 2000.00 | 0.9100 | 2.00 IC | 0.23 IC | | 0.00 | 0.00 | | | | | 0.003 |
| 3.00 | 0,029 | 2000.10 | 9.42 00 | 2.54 IC | 0.00 IC | | 0.00 | 0.00 | | | | | 9.423 |
| 3.00 | 0,714 | 2055.10 | 10.01.00 | 2.55 IC | 7.40 IC | | 0.00 | 0.00 | | | | | 10.01 |
| 3.1Z | 0,099 | 2000.22 | 10.56 00 | 2.50 IC | 0.03 IC | | 0.00 | 0.00 | | | | | 10.00 |
| 3.10 201 | 9,009 | 2000.20 | 11.12.00 | 2.00 10 | 0.04 IC | | 0.00 | 0.00 | | | | | 11.12 |
| 3.04 | 9,240 | 2055.34 | 12 11 00 | 2.00 IC | 9.03 IC | | 0.00 | 0.00 | | | | | 12 11 |
| 3.91 | 9,410 | 2055.41 | 12.11.00 | 2.02 IC | 9.49 IC | | 0.00 | 0.00 | | | | | 12.11 |
| 1.03 | 9,500 | 2055.47 | 12.00 00 | 2.00 IC | 9.93 ic | | 0.00 | 0.00 | | | | | 12.00 |
| 4.00 | 0 021 | 2055.55 | 13.45 oc | 2.07 iC | 10.33 ic | | 0.00 | 0.00 | | | | | 13.02 |
| 4.05 | 10 091 | 2055.55 | 13.45 OC | 2.03 iC | 11 15 ic | | 0.00 | 0.00 | | | | | 13.45 |
| 4.10 | 10,001 | 2055.00 | 14 26 oc | 2.71 ic | 11.10 ic | | 0.00 | 0.00 | | | | | 14 26 |
| 4.22 | 10,202 | 2055 78 | 14.65 oc | 2.70 ic | 11.80 ic | | 0.00 | 0.00 | | | | | 14.20 |
| 4.34 | 10,402 | 2055.84 | 15.03 oc | 2.70 ic | 12 25 ic | | 0.00 | 0.00 | | | | | 15.02 |
| 4 40 | 10,002 | 2055.90 | 15.39 oc | 2.80 ic | 12.59 ic | | 0.00 | 0.00 | | | | | 15.39 |
| 4 46 | 10,868 | 2055.96 | 15 75 oc | 2.82 ic | 12.00 lc | | 0.00 | 0.00 | | | | | 15 75 |
| 4.53 | 11.001 | 2056.03 | 16.10 oc | 2.84 ic | 13.25 ic | | 0.00 | 0.00 | | | | | 16.10 |
| 4.59 | 11,133 | 2056.09 | 16.44 oc | 2.86 ic | 13.57 ic | | 0.00 | 0.00 | | | | | 16.44 |
| 4.65 | 11,266 | 2056.15 | 16.79 oc | 2.88 ic | 13.88 ic | | 0.00 | 0.03 | | | | | 16.79 |
| 4.71 | 11,399 | 2056.21 | 17.18 oc | 2.90 ic | 14.19 ic | | 0.00 | 0.09 | | | | | 17.18 |
| 4.77 | 11,532 | 2056.27 | 17.58 oc | 2.91 ic | 14.49 ic | | 0.00 | 0.18 | | | | | 17.58 |
| 4.84 | 11,664 | 2056.34 | 17.99 oc | 2.93 ic | 14.78 ic | | 0.00 | 0.28 | | | | | 17.99 |
| 4.90 | 11,797 | 2056.40 | 18.40 oc | 2.94 ic | 15.07 ic | | 0.00 | 0.40 | | | | | 18.40 |
| 4.96 | 11,930 | 2056.46 | 18.82 oc | 2.95 ic | 15.35 ic | | 0.00 | 0.52 | | | | | 18.82 |
| 5.02 | 12,031 | 2056.52 | 19.25 oc | 2.96 ic | 15.62 ic | | 0.00 | 0.67 | | | | | 19.25 |
| 5.08 | 12,132 | 2056.58 | 19.69 oc | 2.97 ic | 15.90 ic | | 0.00 | 0.82 | | | | | 19.69 |
| 5.15 | 12,233 | 2056.65 | 20.12 oc | 2.98 ic | 16.16 ic | | 0.00 | 0.98 | | | | | 20.12 |
| 5.21 | 12,333 | 2056.71 | 20.57 oc | 2.99 ic | 16.43 ic | | 0.00 | 1.15 | | | | | 20.56 |
| 5.27 | 12,434 | 2056.77 | 21.01 oc | 2.99 ic | 16.68 ic | | 0.00 | 1.33 | | | | | 21.01 |
| 5.33 | 12,535 | 2056.83 | 21.46 oc | 3.00 ic | 16.94 ic | | 0.00 | 1.52 | | | | | 21.46 |
| 5.39 | 12,636 | 2056.89 | 21.91 oc | 3.00 ic | 17.19 ic | | 0.00 | 1.72 | | | | | 21.91 |
| 5.46 | 12,737 | 2056.96 | 22.36 ic | 3.00 ic | 17.44 ic | | 0.00 | 1.93 | | | | | 22.36 |
| 5.52 | 12,838 | 2057.02 | 22.76 ic | 2.99 ic | 17.64 ic | | 0.00 | 2.14 | | | | | 22.76 |
| 5.58 | 12,939 | 2057.08 | 23.02 ic | 2.99 ic | 17.67 ic | | 0.00 | 2.36 | | | | | 23.02 |
| 5.64 | 13,037 | 2057.14 | 23.29 ic | 3.00 ic | 17.71 ic | | 0.00 | 2.59 | | | | | 23.29 |
| 5.70 | 13,136 | 2057.20 | 23.56 ic | 3.00 ic | 17.73 ic | | 0.00 | 2.82 | | | | | 23.56 |
| 5.77 | 13,235 | 2057.27 | 23.83 ic | 3.01 ic | 17.76 ic | | 0.00 | 3.06 | | | | | 23.83 |
| 5.83 | 13,333 | 2057.33 | 24.10 ic | 3.01 ic | 17.78 ic | | 0.00 | 3.31 | | | | | 24.10 |
| 5.89 | 13,432 | 2057.39 | 24.37 ic | 3.01 ic | 17.79 ic | | 0.00 | 3.56 | | | | | 24.37 |
| 5.95 | 13,531 | 2057.45 | 24.64 ic | 3.02 ic | 17.81 ic | | 0.00 | 3.82 | | | | | 24.64 |
| 6.01 | 13,629 | 2057.51 | 24.92 ic | 3.02 ic | 17.82 ic | | 0.00 | 4.09 | | | | | 24.92 |
| 6.08 | 13,728 | 2057.58 | 25.20 ic | 3.02 ic | 17.82 ic | | 0.00 | 4.36 | | | | | 25.20 |
| 6.14 | 13,827 | 2057.64 | 25.48 ic | 3.02 ic | 17.82 ic | | 0.00 | 4.64 | | | | | 25.48 |
| 6.20 | 13,925 | 2057.70 | 25.76 ic | 3.02 ic | 17.82 ic | | 0.00 | 4.92 | | | | | 25.75 |

...End

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Friday, 04 / 29 / 2022

Hyd. No. 16

Union S. Basin Out

| Hydrograph type = | = Reservoir | Peak discharge | = 3.004 cfs |
|-------------------|---------------------------------|----------------|---------------|
| Storm frequency = | = 1 yrs | Time to peak | = 724 min |
| Time interval = | = 2 min | Hyd. volume | = 23,126 cuft |
| Inflow hyd. No. = | = 15 - Union South Basin Inflow | Max. Elevation | = 2054.50 ft |
| Reservoir name = | Union South Underground Det | tMax. Storage | = 6,746 cuft |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Friday, 04 / 29 / 2022

Hyd. No. 16

Union S. Basin Out

| Hydrograph type | = Reservoir | Peak discharge | = 14.35 cfs |
|-----------------|---------------------------------|----------------|---------------|
| Storm frequency | = 10 yrs | Time to peak | = 720 min |
| Time interval | = 2 min | Hyd. volume | = 45,566 cuft |
| Inflow hyd. No. | = 15 - Union South Basin Inflow | Max. Elevation | = 2055.73 ft |
| Reservoir name | = Union South Underground Det | tMax. Storage | = 10,299 cuft |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 17

Total To 460 South Culvert

| Hydrograph type | = Combine | Peak discharge | = 49.07 cfs |
|-----------------|--------------|----------------------|----------------|
| Storm frequency | = 1 yrs | Time to peak | = 716 min |
| Time interval | = 2 min | Hyd. volume | = 119,154 cuft |
| Inflow hyds. | = 13, 14, 16 | Contrib. drain. area | = 25.030 ac |



Friday, 04 / 29 / 2022

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 17

Total To 460 South Culvert

| Hydrograph type = | - Combine | Peak discharge | = 119.01 cfs |
|-------------------|--------------|----------------------|----------------|
| Storm frequency = | = 10 yrs | Time to peak | = 716 min |
| Time interval = | = 2 min | Hyd. volume | = 275,723 cuft |
| Inflow hyds. | = 13, 14, 16 | Contrib. drain. area | = 25.030 ac |



Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Pond Data

Contours -User-defined contour areas. Average end area method used for volume calculation. Begining Elevation = 2038.00 ft

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 2038.00 | 00 | 0 | 0 |
| 2.00 | 2040.00 | 4,884 | 4,884 | 4,884 |
| 4.00 | 2042.00 | 7,175 | 12,059 | 16,943 |
| 6.00 | 2044.00 | 9,534 | 16,709 | 33,652 |
| 8.00 | 2046.00 | 12,012 | 21,546 | 55,198 |
| 10.00 | 2048.00 | 14,742 | 26,754 | 81,952 |
| 12.00 | 2050.00 | 17,943 | 32,685 | 114,637 |

Culvert / Orifice Structures

| | [A] | [B] | [C] | [PrfRsr] | | [A] | [B] | [C] | [D] |
|-----------------|-----------|------|------|----------|----------------|-------------|-----------|------|------|
| Rise (in) | = 36.00 | 0.00 | 0.00 | 0.00 | Crest Len (ft) | = 0.00 | 0.00 | 0.00 | 0.00 |
| Span (in) | = 36.00 | 0.00 | 0.00 | 0.00 | Crest El. (ft) | = 0.00 | 0.00 | 0.00 | 0.00 |
| No. Barrels | = 1 | 0 | 0 | 0 | Weir Coeff. | = 3.33 | 3.33 | 3.33 | 3.33 |
| Invert El. (ft) | = 2038.00 | 0.00 | 0.00 | 0.00 | Weir Type | = | | | |
| Length (ft) | = 203.10 | 0.00 | 0.00 | 0.00 | Multi-Stage | = No | No | No | No |
| Slope (%) | = 2.92 | 0.00 | 0.00 | n/a | - | | | | |
| N-Value | = .024 | .013 | .013 | n/a | | | | | |
| Orifice Coeff. | = 0.60 | 0.60 | 0.60 | 0.60 | Exfil.(in/hr) | = 0.000 (by | Wet area) | | |
| Multi-Stage | = n/a | No | No | No | TW Elev. (ft) | = 0.00 | . , | | |

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Weir Structures

| Stage / | Storage / | Discharge 1 | Table | | , - | | | | | | | , | .9 (-). |
|-------------|-----------------|-----------------|--------------|--------------|--------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
| 0.00 | 0 | 2038.00 | 0.00 | | | | | | | | | | 0.000 |
| 0.20 | 488 | 2038.20 | 0.31 ic | | | | | | | | | | 0.309 |
| 0.40 | 977 | 2038.40 | 1.21 ic | | | | | | | | | | 1.207 |
| 0.60 | 1,465 | 2038.60 | 2.66 ic | | | | | | | | | | 2.662 |
| 0.80 | 1,954 | 2038.80 | 4.61 ic | | | | | | | | | | 4.610 |
| 1.00 | 2,442 | 2039.00 | 7.03 ic | | | | | | | | | | 7.030 |
| 1.20 | 2,930 | 2039.20 | 9.85 ic | | | | | | | | | | 9.852 |
| 1.40 | 3,419 | 2039.40 | 13.04 ic | | | | | | | | | | 13.04 |
| 1.60 | 3,907 | 2039.60 | 16.53 ic | | | | | | | | | | 16.53 |
| 1.80 | 4,396 | 2039.80 | 20.25 ic | | | | | | | | | | 20.25 |
| 2.00 | 4.884 | 2040.00 | 24.12 ic | | | | | | | | | | 24.12 |
| 2.20 | 6,090 | 2040.20 | 28.08 ic | | | | | | | | | | 28.08 |
| 2.40 | 7,296 | 2040.40 | 31.98 ic | | | | | | | | | | 31.98 |
| 2.60 | 8.502 | 2040.60 | 35.75 ic | | | | | | | | | | 35.75 |
| 2.80 | 9,708 | 2040.80 | 39.12 ic | | | | | | | | | | 39.12 |
| 3.00 | 10,914 | 2041.00 | 41.68 ic | | | | | | | | | | 41.68 |
| 3.20 | 12,119 | 2041.20 | 44.37 ic | | | | | | | | | | 44.37 |
| 3.40 | 13,325 | 2041.40 | 46.91 ic | | | | | | | | | | 46.91 |
| 3.60 | 14,531 | 2041.60 | 49.32 ic | | | | | | | | | | 49.32 |
| 3.80 | 15,737 | 2041.80 | 51.61 ic | | | | | | | | | | 51.61 |
| 4.00 | 16,943 | 2042.00 | 53.81 ic | | | | | | | | | | 53.81 |
| 4.20 | 18,614 | 2042.20 | 55.92 ic | | | | | | | | | | 55.92 |
| 4.40 | 20,285 | 2042.40 | 57.95 ic | | | | | | | | | | 57.95 |
| 4.60 | 21,956 | 2042.60 | 59.92 ic | | | | | | | | | | 59.92 |
| 4.80 | 23,627 | 2042.80 | 61.82 ic | | | | | | | | | | 61.82 |
| 5.00 | 25,298 | 2043.00 | 62.77 oc | | | | | | | | | | 62.77 |
| 5.20 | 26,968 | 2043.20 | 63.56 oc | | | | | | | | | | 63.56 |
| 5.40 | 28,639 | 2043.40 | 64.33 oc | | | | | | | | | | 64.33 |
| 5.60 | 30,310 | 2043.60 | 65.10 oc | | | | | | | | | | 65.10 |
| 5.80 | 31,981 | 2043.80 | 65.86 oc | | | | | | | | | | 65.86 |
| 6.00 | 33,652 | 2044.00 | 66.61 oc | | | | | | | | | | 66.61 |
| 6.20 | 35.807 | 2044.20 | 67.35 oc | | | | | | | | | | 67.35 |
| 6.40 | 37,961 | 2044.40 | 68.09 oc | | | | | | | | | | 68.09 |
| 6.60 | 40,116 | 2044.60 | 68.81 oc | | | | | | | | | | 68.81 |
| 6.80 | 42,270 | 2044.80 | 69.53 oc | | | | | | | | | | 69.53 |
| 7 00 | 44 425 | 2045 00 | 70 24 00 | | | | | | | | | | 70 24 |

Friday, 04 / 29 / 2022

460 South Culvert HW Storage Stage / Storage / Discharge Table

| • | • | • | | | | | | | | | | | |
|-------------|-----------------|-----------------|--------------|--------------|--------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
| 7.20 | 46,580 | 2045.20 | 70.95 oc | | | | | | | | | | 70.95 |
| 7.40 | 48,734 | 2045.40 | 71.64 oc | | | | | | | | | | 71.64 |
| 7.60 | 50,889 | 2045.60 | 72.33 oc | | | | | | | | | | 72.33 |
| 7.80 | 53,043 | 2045.80 | 73.02 oc | | | | | | | | | | 73.02 |
| 8.00 | 55,198 | 2046.00 | 73.69 oc | | | | | | | | | | 73.69 |
| 8.20 | 57,873 | 2046.20 | 74.36 oc | | | | | | | | | | 74.36 |
| 8.40 | 60,549 | 2046.40 | 75.03 oc | | | | | | | | | | 75.03 |
| 8.60 | 63,224 | 2046.60 | 75.69 oc | | | | | | | | | | 75.69 |
| 8.80 | 65,900 | 2046.80 | 76.34 oc | | | | | | | | | | 76.34 |
| 9.00 | 68,575 | 2047.00 | 76.99 oc | | | | | | | | | | 76.99 |
| 9.20 | 71,250 | 2047.20 | 77.63 oc | | | | | | | | | | 77.63 |
| 9.40 | 73,926 | 2047.40 | 78.27 oc | | | | | | | | | | 78.27 |
| 9.60 | 76,601 | 2047.60 | 78.90 oc | | | | | | | | | | 78.90 |
| 9.80 | 79,277 | 2047.80 | 79.53 oc | | | | | | | | | | 79.53 |
| 10.00 | 81,952 | 2048.00 | 80.15 oc | | | | | | | | | | 80.15 |
| 10.20 | 85,221 | 2048.20 | 80.77 oc | | | | | | | | | | 80.77 |
| 10.40 | 88,489 | 2048.40 | 81.38 oc | | | | | | | | | | 81.38 |
| 10.60 | 91,758 | 2048.60 | 81.99 oc | | | | | | | | | | 81.99 |
| 10.80 | 95,026 | 2048.80 | 82.60 oc | | | | | | | | | | 82.60 |
| 11.00 | 98,295 | 2049.00 | 83.19 oc | | | | | | | | | | 83.19 |
| 11.20 | 101,563 | 2049.20 | 83.79 oc | | | | | | | | | | 83.79 |
| 11.40 | 104,832 | 2049.40 | 84.38 oc | | | | | | | | | | 84.38 |
| 11.60 | 108,100 | 2049.60 | 84.97 oc | | | | | | | | | | 84.97 |
| 11.80 | 111,369 | 2049.80 | 85.55 oc | | | | | | | | | | 85.55 |
| 12.00 | 114,637 | 2050.00 | 86.13 oc | | | | | | | | | | 86.13 |
| | | | | | | | | | | | | | |

...End

95



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 18

460 South Culvert Out

| Hydrograph type | = Reservoir | Peak discharge | = 40.17 cfs |
|-----------------------------------|---|-----------------------------------|-------------------------------|
| Time interval | $= 2 \min$ | Hyd. volume | = 119,153 cuft |
| Inflow hyd. No. Reservoir name | = 17 - Total To 460 South Culve= 460 South Culvert HW Storag | enMax. Elevation eMax. Storage | = 2040.88 ft = 10,199 cuft |

Storage Indication method used.



Friday, 04 / 29 / 2022

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Friday, 04 / 29 / 2022

Hyd. No. 18

460 South Culvert Out

| Hydrograph type = | = Reservoir | Peak discharge | = 68.09 cfs |
|-------------------|---------------------------------|-----------------|----------------|
| Storm frequency = | = 10 yrs | Time to peak | = 722 min |
| Time interval : | = 2 min | Hyd. volume | = 275,721 cuft |
| Inflow hyd. No. | = 17 - Total To 460 South Culve | nMax. Elevation | = 2044.40 ft |
| Reservoir name | = 460 South Culvert HW Storage | eMax. Storage | = 37,977 cuft |





- VARIABLE WIDTH PRIVATE STORM WATER MANAGEMENT EASEMENT

60 FEET HEET NUMBER 1 OF 1

| The proji repr with | GAY AND NEEL, INC. ■ BORNEDINA + UND THERE, INC. | ue contraction of the contractio | Phone: (540) 381-6011 Fax: (540) 381-2773 Fax: (540) 381-2773 Fax: fish (540) 281-2773 | www.gayandheel.com |
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| | POST-DEVELOPMENT DA MAP | | THE FARM | TOWN OF BLACKSBURG, VIRGINIA |
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| | GRAPHIC | C SCALE | F |
| | CONTOUR INTE | RVAL = 1 FT. | |

Drainage Area Runoff and Time of Concentration

| Precipitation Data | | | | | | | |
|--------------------|---------|--|--|--|--|--|--|
| Return | | | | | | | |
| Frequency | P (in.) | | | | | | |
| 1 Yr. | 2.26 | | | | | | |
| 2 Yr. | 2.73 | | | | | | |
| 10 Yr. | 4.06 | | | | | | |
| 100 Yr. | 6.44 | | | | | | |

| Drainage Area: | "The Farm" Dr | ainage / | Areas | | | | | | | | | |
|-----------------|-----------------|-------------|--|-------------------------|--------------------|--------------|-----------------------|--------------|-----------|-------------------|---------------------|----------------------|
| | Comr | posite Cr | urve Number (| (CN) | l | | ٦ | Time of Con | centratio | n, T _c | | |
| | | | , | | l | | | Τ | | | | Travel |
| | | ' | | 1 1 | l | Flow | | Land | Length | Roughness | Slope | Time, T _t |
| | | CN | Area (Ac.) | CN*A | | Segment | Flow Regime | Cover | (ft) | Coeff., n | (ft/ft) | (min.) |
| | CN ₁ | 79 | 0.55 | 43.45 | l | 1 | | | | | | |
| | CN ₂ | 75 | 0.77 | 57.75 | l | 2 | | | | | | |
| | CN ₃ | | | 0.00 | l | 3 | | | | | | |
| | CN ₄ | 1 | | 0.00 | l | 4 | | | | | | |
| | CN ₅ | 1 | | 0.00 | l | 5 | | | | | | |
| Undetained | Total | - | 1.32 | 101.20 | l | 6 | Other Tt | | | | | 8.6 |
| areas total | | Co | mposite CN = | 77 | l | | | Total Tim | ne of Con | centration, T | _c (min.) | 8.6 |
| | | | | | | | | | | | | |
| | | | | Kunon | 1 Vr | 10 Vr | 100 Vr | - | | | | |
| | | Com | nosite (N | | 1 Yr. 77 | 77 | 77 | | | | | |
| | Stc | vrage (in |) S=1000/CN- | 10 | 2,99 | 2,99 | 2,99 | 4 | | | | |
| | | al abstra | $\frac{1}{2} \int \frac{1}{2} \int \frac{1}$ | 125 | 0.60 | 0.60 | 0.60 | - | | | | |
| | Bunoff de | n ubstra | $\frac{1}{1000} - (0.025)^2/$ | .25 [/p \±S] | 0.00 | 1 86 | 2.97 | - | | | | |
| | Runoff | | $\frac{1}{(200 \text{ ft}) \text{ RV} = 0}$ | (P-1a/T-3) /10*A | 0.35 | 1.00 0.20 | 0.43 | - | | | | |
| | Flow rat | volume | $\frac{ac-n}{r}$, $nv - w$ | /12°A | 1.20 | 3.89 | 0.45 | Hydrogra | nh No.: | Contributes | to 21 | |
| | Notes | See "Th | peak nonnyan | hy others (N | 1=D41 post | weighted C | N CN2=DA3 pos | t weighted (| см | | | |
| | Notes. | | | by others. ert. | <u>1-0/11 post</u> | Weighter e | <u>N, CN2-DN3 p03</u> | t Weighten (| | | | |
| | Com | posite C | urve Number (| (CN) | | 1 | | Time of Con | centratio | n, T _c | | |
| | | | | | l | | | Τ | | | | Travel |
| | | ' | | 1 | l | Flow | | Land | Length | Roughness | Slope | Time, T _t |
| | | CN | Area (Ac.) | CN*A | | Segment | Flow Regime | Cover | (ft) | Coeff., n | (ft/ft) | (min.) |
| | CN ₁ | 91 | 2.67 | 242.97 | | 1 | | | | | | |
| | CN ₂ | | | 0.00 | l | 2 | | | | | | |
| | CN ₃ | | | 0.00 | l | 3 | | | | | | |
| | CN ₄ | | | 0.00 | l | 4 | | | | | | |
| | CN ₅ | | | 0.00 | l | 5 | | | | | | |
| Area to "The | Total | - | 2.67 | 242.97 | | 6 | Other Tt | | | | | 5.8 |
| Farm" detention | | Co | mposite CN = | 91 | l | | | Total Tim | ne of Con | centration, T | _c (min.) | 5.8 |
| | | | | Runoff | | | | Г | | | | |
| 1 | | | | 1 | 1 Yr. | 10 Yr. | 100 Yr. | - | | | | |
| 1 | | VR | RM CN* | | 91 | 91 | 91 | *If differer | nt from C | omposite CN | , runoff | reduction |
| 1 | Sto | orage (in | .) S=1000/CN-? | 10 | 0.99 | 0.99 | 0.99 | BMPs are | utilized | · | | |
| | Initia | al abstra | ction (in.), I _a =C | J.2S | 0.20 | 0.20 | 0.20 | 1 | | | | |
| | Runoff de | epth (in.) |), Q=(P-0.2S) ² / | [(P-I _a)+S] | 1.39 | 3.07 | 5.39 | 1 | | | | |
| | Runoff | volume | (ac-ft), RV = Q | /12*A | 0.31 | 0.68 | 1.20 | 1 | | | | |
| | Flow rat | :e (cfs), c | a _{peak} from hydr | ograph | 6.19 | 13.12 | | Hydrogra | aph No.: | 19 | | |
| | Notes: | See "Th | ne Farm" calcs | by others. CN | 1=DA3 post | weighted C | .N | _ · - | | | • | |

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 19

The Farm Basin Inflow

| Hydrograph type | = SCS Runoff | Peak discharge | = 6.187 cfs |
|-----------------|--------------|--------------------|---------------|
| Storm frequency | = 1 yrs | Time to peak | = 716 min |
| Time interval | = 2 min | Hyd. volume | = 12,664 cuft |
| Drainage area | = 2.670 ac | Curve number | = 91 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 5.80 min |
| Total precip. | = 2.26 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



Friday, 04 / 29 / 2022

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 19

The Farm Basin Inflow

| Hydrograph type | = SCS Runoff | Peak discharge | = 13.12 cfs |
|-----------------|--------------|--------------------|---------------|
| Storm frequency | = 10 yrs | Time to peak | = 716 min |
| Time interval | = 2 min | Hyd. volume | = 27,939 cuft |
| Drainage area | = 2.670 ac | Curve number | = 91 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 5.80 min |
| Total precip. | = 4.06 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Pond Data

Pond storage is based on user-defined values.

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 2080.85 | n/a | 0 | 0 |
| 0.05 | 2080.90 | n/a | 126 | 126 |
| 0.24 | 2081.09 | n/a | 428 | 554 |
| 0.41 | 2081.26 | n/a | 406 | 960 |
| 0.69 | 2081.54 | n/a | 632 | 1,592 |
| 0.96 | 2081.81 | n/a | 1,180 | 2,772 |
| 1.53 | 2082.38 | n/a | 2,806 | 5,578 |
| 2.21 | 2083.06 | n/a | 3,199 | 8,777 |
| 2.63 | 2083.48 | n/a | 1,937 | 10,714 |
| 2.82 | 2083.67 | n/a | 835 | 11,549 |
| 3.40 | 2084.25 | n/a | 2,383 | 13,932 |
| 3.97 | 2084.82 | n/a | 2,068 | 16,000 |
| 4.40 | 2085.25 | n/a | 2,390 | 18,390 |
| 5.50 | 2086.35 | n/a | 1,362 | 19,752 |
| | | | | |

Culvert / Orifice Structures

Weir Structures

| | [A] | [B] | [C] | [PrfRsr] | | [A] | [B] | [C] | [D] |
|-----------------|-----------|---------|---------|----------|----------------|---------------|-----------|------|------|
| Rise (in) | = 15.00 | 1.00 | 5.00 | 0.00 | Crest Len (ft) | = 3.93 | 30.00 | 0.00 | 0.00 |
| Span (in) | = 15.00 | 1.00 | 5.00 | 0.00 | Crest El. (ft) | = 2085.25 | 2086.00 | 0.00 | 0.00 |
| No. Barrels | = 1 | 1 | 2 | 0 | Weir Coeff. | = 3.33 | 3.33 | 3.33 | 3.33 |
| Invert El. (ft) | = 2080.85 | 2080.85 | 2083.85 | 0.00 | Weir Type | = 1 | Broad | | |
| Length (ft) | = 120.00 | 0.00 | 0.00 | 0.00 | Multi-Stage | = Yes | No | No | No |
| Slope (%) | = 0.00 | 0.00 | 0.00 | n/a | | | | | |
| N-Value | = .013 | .013 | .013 | n/a | | | | | |
| Orifice Coeff. | = 0.70 | 0.60 | 0.60 | 0.60 | Exfil.(in/hr) | = 0.000 (by V | Vet area) | | |
| Multi-Stage | = n/a | Yes | Yes | No | TW Elev. (ft) | = 0.00 | | | |

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s). Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| | | - | | | | | | | | | | | |
| 0.00 | 0 | 2080.85 | 0.00 | 0.00 | 0.00 | | 0.00 | 0.00 | | | | | 0.000 |
| 0.00 | 13 | 2080.85 | 0.00 ic | 0.00 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.000 |
| 0.01 | 25 | 2080.86 | 0.00 ic | 0.00 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.000 |
| 0.01 | 38 | 2080.86 | 0.00 ic | 0.00 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.000 |
| 0.02 | 50 | 2080.87 | 0.00 ic | 0.00 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.001 |
| 0.03 | 63 | 2080.88 | 0.00 ic | 0.00 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.001 |
| 0.03 | 76 | 2080.88 | 0.00 ic | 0.00 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.001 |
| 0.04 | 88 | 2080.88 | 0.00 ic | 0.00 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.001 |
| 0.04 | 101 | 2080.89 | 0.00 ic | 0.00 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.002 |
| 0.04 | 113 | 2080.89 | 0.00 ic | 0.00 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.002 |
| 0.05 | 126 | 2080.90 | 0.00 ic | 0.00 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.003 |
| 0.07 | 169 | 2080.92 | 0.00 ic | 0.00 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.004 |
| 0.09 | 212 | 2080.94 | 0.01 ic | 0.01 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.006 |
| 0.11 | 254 | 2080.96 | 0.01 ic | 0.01 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.007 |
| 0.13 | 297 | 2080.98 | 0.01 ic | 0.01 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.008 |
| 0.14 | 340 | 2081.00 | 0.01 ic | 0.01 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.008 |
| 0.16 | 383 | 2081.01 | 0.01 ic | 0.01 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.009 |
| 0.18 | 426 | 2081.03 | 0.01 ic | 0.01 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.010 |
| 0.20 | 468 | 2081.05 | 0.01 ic | 0.01 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.011 |
| 0.22 | 511 | 2081.07 | 0.01 ic | 0.01 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.011 |
| 0.24 | 554 | 2081.09 | 0.01 ic | 0.01 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.012 |
| 0.26 | 595 | 2081.11 | 0.01 ic | 0.01 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.012 |
| 0.27 | 635 | 2081.12 | 0.01 ic | 0.01 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.013 |
| 0.29 | 676 | 2081 14 | 0.01 ic | 0.01 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.013 |
| 0.31 | 716 | 2081 16 | 0.01 ic | 0.01 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.013 |
| 0.32 | 757 | 2081 18 | 0.01 ic | 0.01 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.014 |
| 0.34 | 798 | 2081.10 | 0.01 ic | 0.01 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.014 |
| 0.36 | 838 | 2081 21 | 0.01 ic | 0.01 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.015 |
| 0.38 | 870 | 2081.21 | 0.07 ic | 0.01 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.015 |
| 0.30 | 019 | 2001.20 | 0.02 ic | 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.015 |
| 0.59 | 919 | 2001.24 | 0.02 10 | 0.02 10 | 0.00 | | 0.00 | 0.00 | | | | | 0.015 |

The Farm Underground Det Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|--------------|-----------------|-----------------|--------------------|--------------------|--------------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| 0.41 | 960 | 2081.26 | 0.02 ic | 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.016 |
| 0.44 | 1,023 | 2081.29 | 0.02 ic | 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.016 |
| 0.47 | 1,086 | 2081.32 | 0.02 ic | 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.017 |
| 0.49 | 1,150 | 2081.34 | 0.02 ic | 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.017 |
| 0.52 | 1,213 | 2081.37 | 0.02 ic | 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.018 |
| 0.55 | 1,270 | 2081.40 | 0.02 lC | 0.02 IC 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.018 |
| 0.50 | 1,339 | 2081.45 | 0.02 ic | 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.019 |
| 0.63 | 1,466 | 2081.49 | 0.02 ic | 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.020 |
| 0.66 | 1,529 | 2081.51 | 0.02 ic | 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.020 |
| 0.69 | 1,592 | 2081.54 | 0.02 ic | 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.021 |
| 0.72 | 1,710 | 2081.57 | 0.02 ic | 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.021 |
| 0.74 | 1,828 | 2081.59 | 0.02 ic | 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.022 |
| 0.77 | 1,946 | 2081.62 | 0.02 ic | 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.022 |
| 0.80 | 2,064 | 2081.65 | 0.02 IC | 0.02 IC | 0.00 | | 0.00 | 0.00 | | | | | 0.023 |
| 0.62 | 2,102 | 2001.00 | 0.02 lC | 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.023 |
| 0.00 | 2,300 | 2081.70 | 0.02 ic | 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.023 |
| 0.91 | 2,536 | 2081.76 | 0.03 ic | 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.024 |
| 0.93 | 2,654 | 2081.78 | 0.03 ic | 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.024 |
| 0.96 | 2,772 | 2081.81 | 0.03 ic | 0.02 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.025 |
| 1.02 | 3,053 | 2081.87 | 0.03 ic | 0.03 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.026 |
| 1.07 | 3,333 | 2081.92 | 0.03 ic | 0.03 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.026 |
| 1.13 | 3,614 | 2081.98 | 0.03 ic | 0.03 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.027 |
| 1.19 | 3,894 | 2082.04 | 0.03 ic | 0.03 IC | 0.00 | | 0.00 | 0.00 | | | | | 0.028 |
| 1.25 | 4,175 | 2082.09 | 0.03 IC | 0.03 IC | 0.00 | | 0.00 | 0.00 | | | | | 0.028 |
| 1.30 | 4,430 | 2082.15 | 0.03 ic | 0.03 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.029 |
| 1.00 | 5 017 | 2082.21 | 0.03 ic | 0.03 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.030 |
| 1.47 | 5,297 | 2082.32 | 0.03 ic | 0.03 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.031 |
| 1.53 | 5,578 | 2082.38 | 0.03 ic | 0.03 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.032 |
| 1.60 | 5,898 | 2082.45 | 0.03 ic | 0.03 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.032 |
| 1.67 | 6,218 | 2082.52 | 0.03 ic | 0.03 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.033 |
| 1.73 | 6,538 | 2082.58 | 0.03 ic | 0.03 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.034 |
| 1.80 | 6,858 | 2082.65 | 0.03 ic | 0.03 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.035 |
| 1.87 | 7,178 | 2082.72 | 0.04 IC | 0.04 IC | 0.00 | | 0.00 | 0.00 | | | | | 0.035 |
| 2.01 | 7,497 | 2082.79 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.030 |
| 2.01 | 8 137 | 2082.00 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.037 |
| 2.14 | 8.457 | 2082.99 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.038 |
| 2.21 | 8,777 | 2083.06 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.038 |
| 2.25 | 8,971 | 2083.10 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.039 |
| 2.29 | 9,164 | 2083.14 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.039 |
| 2.34 | 9,358 | 2083.19 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.039 |
| 2.38 | 9,552 | 2083.23 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.040 |
| 2.42 | 9,746 | 2083.27 | 0.04 IC | 0.04 IC | 0.00 | | 0.00 | 0.00 | | | | | 0.040 |
| 2.40 | 9,939 | 2003.31 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.041 |
| 2.50 | 10,133 | 2003.33 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.041 |
| 2.59 | 10,520 | 2083.44 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.042 |
| 2.63 | 10,714 | 2083.48 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.042 |
| 2.65 | 10,798 | 2083.50 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.042 |
| 2.67 | 10,881 | 2083.52 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.042 |
| 2.69 | 10,965 | 2083.54 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.042 |
| 2.71 | 11,048 | 2083.56 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.043 |
| 2.72 | 11,132 | 2083.57 | 0.04 ic | 0.04 IC | 0.00 | | 0.00 | 0.00 | | | | | 0.043 |
| 2.74 | 11,215 | 2083.59 | 0.04 IC | 0.04 IC | 0.00 | | 0.00 | 0.00 | | | | | 0.043 |
| 2.70 | 11,299 | 2003.01 | 0.04 IC | 0.04 IC | 0.00 | | 0.00 | 0.00 | | | | | 0.043 |
| 2.70 | 11 466 | 2083.65 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.043 |
| 2.82 | 11.549 | 2083.67 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.043 |
| 2.88 | 11,787 | 2083.73 | 0.04 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.044 |
| 2.94 | 12,026 | 2083.79 | 0.05 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.044 |
| 2.99 | 12,264 | 2083.84 | 0.05 ic | 0.04 ic | 0.00 | | 0.00 | 0.00 | | | | | 0.045 |
| 3.05 | 12,502 | 2083.90 | 0.07 ic | 0.05 ic | 0.02 ic | | 0.00 | 0.00 | | | | | 0.061 |
| 3.11 | 12,741 | 2083.96 | 0.12 ic | 0.05 ic | 0.07 ic | | 0.00 | 0.00 | | | | | 0.111 |
| 3.17 | 12,979 | 2084.02 | 0.20 ic | 0.05 ic | 0.15 ic | | 0.00 | 0.00 | | | | | 0.191 |
| 3.23 | 13,217 | 2084.08 | 0.30 IC | 0.05 IC | 0.25 10 | | 0.00 | 0.00 | | | | | 0.293 |
| 3.20 3.21 | 13,455 | 2084.14 | 0.41 IC 0.53 io | 0.05 IC | 0.30 IC | | 0.00 | 0.00 | | | | | 0.407 |
| 3 40 | 13,094 | 2004.19 | 0.00 ic | 0.05 ic | 0.40 IC 0.58 ic | | 0.00 | 0.00 | | | | | 0.020 |
| 3.46 | 14.139 | 2084.31 | 0.72 ic | 0.05 ic | 0.65 ic | | 0.00 | 0.00 | | | | | 0.701 |
| | ., | | | | | | | | | | | | |

Continues on next page ...

The Farm Underground Det Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| 3 51 | 14 346 | 2084 36 | 0 79 ic | 0 05 ic | 0 73 ic | | 0.00 | 0.00 | | | | | 0 772 |
| 3 57 | 14 552 | 2084 42 | 0.86 ic | 0.05 ic | 0 79 ic | | 0.00 | 0.00 | | | | | 0.837 |
| 3 63 | 14 759 | 2084 48 | 0.90 ic | 0.05 ic | 0.85 ic | | 0.00 | 0.00 | | | | | 0.898 |
| 3.68 | 14 966 | 2084 53 | 0.97 ic | 0.05 ic | 0.91 ic | | 0.00 | 0.00 | | | | | 0.953 |
| 3.74 | 15,173 | 2084.59 | 1.01 ic | 0.05 ic | 0.96 ic | | 0.00 | 0.00 | | | | | 1.006 |
| 3 80 | 15 380 | 2084 65 | 1 06 ic | 0.05 ic | 1 01 ic | | 0.00 | 0.00 | | | | | 1 056 |
| 3.86 | 15,586 | 2084.71 | 1.10 ic | 0.05 ic | 1.06 ic | | 0.00 | 0.00 | | | | | 1.104 |
| 3.91 | 15,793 | 2084.76 | 1.18 ic | 0.05 ic | 1.10 ic | | 0.00 | 0.00 | | | | | 1.150 |
| 3.97 | 16.000 | 2084.82 | 1.22 ic | 0.05 ic | 1.15 ic | | 0.00 | 0.00 | | | | | 1.195 |
| 4.01 | 16.239 | 2084.86 | 1.23 ic | 0.05 ic | 1.18 ic | | 0.00 | 0.00 | | | | | 1.227 |
| 4.06 | 16,478 | 2084.91 | 1.27 ic | 0.05 ic | 1.21 ic | | 0.00 | 0.00 | | | | | 1.258 |
| 4.10 | 16,717 | 2084.95 | 1.31 ic | 0.05 ic | 1.24 ic | | 0.00 | 0.00 | | | | | 1.289 |
| 4.14 | 16,956 | 2084.99 | 1.32 ic | 0.05 ic | 1.27 ic | | 0.00 | 0.00 | | | | | 1.319 |
| 4.19 | 17,195 | 2085.03 | 1.36 ic | 0.05 ic | 1.30 ic | | 0.00 | 0.00 | | | | | 1.348 |
| 4.23 | 17,434 | 2085.08 | 1.41 ic | 0.05 ic | 1.33 ic | | 0.00 | 0.00 | | | | | 1.376 |
| 4.27 | 17,673 | 2085.12 | 1.41 ic | 0.05 ic | 1.35 ic | | 0.00 | 0.00 | | | | | 1.404 |
| 4.31 | 17,912 | 2085.16 | 1.45 ic | 0.05 ic | 1.38 ic | | 0.00 | 0.00 | | | | | 1.432 |
| 4.36 | 18,151 | 2085.21 | 1.46 ic | 0.05 ic | 1.41 ic | | 0.00 | 0.00 | | | | | 1.458 |
| 4.40 | 18,390 | 2085.25 | 1.50 ic | 0.05 ic | 1.43 ic | | 0.00 | 0.00 | | | | | 1.485 |
| 4.51 | 18,526 | 2085.36 | 2.03 ic | 0.05 ic | 1.50 ic | | 0.48 | 0.00 | | | | | 2.028 |
| 4.62 | 18,662 | 2085.47 | 2.98 ic | 0.05 ic | 1.56 ic | | 1.35 | 0.00 | | | | | 2.961 |
| 4.73 | 18,799 | 2085.58 | 4.17 ic | 0.05 ic | 1.62 ic | | 2.48 | 0.00 | | | | | 4.152 |
| 4.84 | 18,935 | 2085.69 | 5.54 oc | 0.04 ic | 1.68 ic | | 3.82 | 0.00 | | | | | 5.535 |
| 4.95 | 19,071 | 2085.80 | 5.63 oc | 0.04 ic | 1.73 ic | | 3.85 ic | 0.00 | | | | | 5.626 |
| 5.06 | 19,207 | 2085.91 | 6.05 oc | 0.04 ic | 1.79 ic | | 4.22 ic | 0.00 | | | | | 6.045 |
| 5.17 | 19,343 | 2086.02 | 6.43 oc | 0.04 ic | 1.84 ic | | 4.56 ic | 0.30 | | | | | 6.739 |
| 5.28 | 19,480 | 2086.13 | 6.77 oc | 0.04 ic | 1.86 ic | | 4.87 ic | 4.74 | | | | | 11.51 |
| 5.39 | 19,616 | 2086.24 | 7.04 oc | 0.04 ic | 1.84 ic | | 5.17 ic | 11.82 | | | | | 18.86 |
| 5.50 | 19,752 | 2086.35 | 7.29 oc | 0.04 ic | 1.81 ic | | 5.44 ic | 20.69 | | | | | 27.99 |

...End

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Tuesday, 11 / 1 / 2022

Hyd. No. 20

The Farm Det. Out

| Hydrograph type = | = Reservoir | Peak discharge | = 0.042 cfs |
|-------------------|------------------------------|----------------|---------------|
| Storm frequency = | = 1 yrs | Time to peak | = 1442 min |
| Time interval : | = 2 min | Hyd. volume | = 10,338 cuft |
| Inflow hyd. No. | = 19 - The Farm Basin Inflow | Max. Elevation | = 2083.50 ft |
| Reservoir name | = The Farm Underground Det | Max. Storage | = 10,783 cuft |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Tuesday, 11 / 1 / 2022

Hyd. No. 20

The Farm Det. Out

| Hydrograph type | = Reservoir | Peak discharge | = 1.203 cfs |
|-----------------|------------------------------|----------------|---------------|
| Storm frequency | = 10 yrs | Time to peak | = 744 min |
| Time interval | = 2 min | Hyd. volume | = 24,576 cuft |
| Inflow hyd. No. | = 19 - The Farm Basin Inflow | Max. Elevation | = 2084.83 ft |
| Reservoir name | = The Farm Underground Det | Max. Storage | = 16,058 cuft |

Drainage Area Runoff and Time of Concentration

| Precipitation Data | | | | |
|--------------------|---------|--|--|--|
| Return | | | | |
| Frequency | P (in.) | | | |
| 1 Yr. | 2.26 | | | |
| 2 Yr. | 2.73 | | | |
| 10 Yr. | 4.06 | | | |
| 100 Yr. | 6.44 | | | |

| The farm "Dribuse is used in the family of | | | | | | | | | | | | | | | |
|--|---|-----------------|------------|---|--|------------|---------------|----------------|--------------|--------------|-------------------|---------------------|----------------------|--|--|
| Tree of Concentration, T _c Composite Curve Number (CN) Travel CN Area (Ac.) CN ^A CN 75 0.57 77.5 CN 75 0.77 57.75 CN 75 0.77 57.75 CN 70 0.55 1 1 CN 1.32 0.000 3 2 | Drainage Area: | "The Farm" Dr | rainage / | Areas | | | | | | | | | | | |
| Undetailed areas total CN Area (A.C.) CN*A CN Area (A.C.) CN*A Soft 1 Land Length Roughness Slope Time, Tr, (N/T) CN 75 0.77 57.75 1 2 | | Com | posite C | urve Number (| (CN) | l | | ٦ | Time of Con | centratio | n, T _c | | | | |
| Image: State in the state in thestate in the state in the state in the state in the st | | | | | | l | | | | | | | Travel | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | | | l | Flow | | Land | Length | Roughness | Slope | Time, T _t | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | CN | Area (Ac.) | CN*A | | Segment | Flow Regime | Cover | (ft) | Coeff., n | (ft/ft) | (min.) | | |
| CN 75 0.7 57.75 CN 0.00 CN 2 1 <th1< th=""> <th1< th=""> <th1< th=""></th1<></th1<></th1<> | | CN ₁ | 79 | 0.55 | 43.45 | l | 1 | | | | | | | | |
| Undetailed areas total CN3 0.00 CN4 0.00 CN3 0.00 CN4 0.00 CN3 0.00 CN4 0.00 CN3 0.00 Total 1.32 101.20 Composite CN = 77 Storage (in,) S=1000/(N-10 2.99 2.99 Initial abstraction (in,), 1=0.25 0.60 0.60 Runoff volume (ac-ft), RV = Q/12*A 0.07 0.20 0.43 Flow rate (r5), g _{pen} , from hydrograph 1.20 3.89 Hydrograph No.: Contributes to 21 Notes: See The Farm' calcs by others. CN1=DA1 post weighted CN, CN2=DA3 post weighted CN Travel CN1 91 2.67 242.97 CN3 0.00 3 Cover (t1) Cert, (trin, 0, (trin, 0) CN4 0.00 3 Cover (t1) Cert, (trin, 0) CN3 0.00 3 Cover (t1) Segment Flow Regime CON3 0.00 3 Cover (t1) Cert, (trin) S.8 <tr< td=""><td></td><td>CN₂</td><td>75</td><td>0.77</td><td>57.75</td><td>l</td><td>2</td><td></td><td></td><td></td><td></td><td></td><td></td></tr<> | | CN ₂ | 75 | 0.77 | 57.75 | l | 2 | | | | | | | | |
| Undetained areas total CN ₁ 0.00 0.00 Total - 1.32 101.20 Composite CN = 77 Composite CN = 77 Composite CN = 77 Storage (in,) S=1000/CN-10 2.99 2.99 Initial abstraction (in,), I ₂ -0.25 0.60 0.60 Runoff depti (in), Q=(P-0.25)?((P-1)/2.45 0.07 0.20 0.43 Flow rate (cS), Q _{mask} from hydrograph 1.20 3.89 Hydrograph No: Contributes to 21 Notes: See "The Farm" calcs by others. CN1=DA1 post weighted CN. Notes: Sione Contributes to 21 Flow rate (cS), Q _{mask} from hydrograph 1.20 3.89 Hydrograph No: Contributes to 21 Notes: See "The Farm" calcs by others. CN1=DA1 post weighted CN. Notes: Sione Travel Flow Regime Cover (ft) Coeff., n (ft/ft) CN Area (AC.) CN*A 0.000 GN 4 I I I I I I I I I I I I | | CN ₃ | | | 0.00 | l | 3 | | | | | | | | |
| Undetained areas total CN3 I IOLO Total - 1.32 101.20 6 Other Tt I 8.5 Generational Composite CN = 77 Tr Total 8.6 Composite CN 77 77 77 77 8.6 Storage (In,) 5=1000/CN+10 2.99 2.99 2.99 1.86 3.87 Runoff volume (ac-ft), RV = Q/12^A 0.07 0.02 0.43 4.8 4.8 Flow rate (CS), Quash for hydrograph 1.20 3.89 Hydrograph No:: Contributes to 21 Notes: See "The Farm" calcs by others. CN1=DA1 post weighted CN, CN2=DA3 post weighted CN Hydrograph No:: Contributes to 21 Notes: See "The Farm" calcs by others. CN1=DA1 post weighted CN, CN2=DA3 post weighted CN, CO2 (ft, 1) Coeff., 1 (ft/ft) CN Area (AC.) CN*A Composite Curve Number (CN) Segment Flow Regime Coeff., 1 (ft/ft) CN Area (AC.) CN*A 0.000 CN I I I I I I | | CN ₄ | | | 0.00 | l | 4 | | | | | | | | |
| Undetained areas total Total - 1.32 101.20 Image: Storage (in:) S=1000/CN:10 77 10 Yr. 100 Yr. Total Time of Concentration, T _c (min.) 8.6 Image: Storage (in:) S=1000/CN:10 2.99 2.99 2.99 1.010 Yr. 100 Yr. Image: Storage (in:) S=1000/CN:10 2.99 2.99 2.99 2.99 1.0120 8.6 Runoff depth (in.), 2(=P0.25)? (IPL)+(S) 0.50 0.60 0.60 0.60 0.60 Runoff depth (in.), 2(=P0.25)? (IPL)+(S) 0.59 1.86 3.87 Hydrograph No.: Contributes to 21 Notes: See "The Farm" calcs by others. CN1=DA1 post weighted CN, CN2=DA3 post weighted CN Hydrograph No.: Contributes to 21 Notes: See "The Farm" calcs by others. CN1=DA1 post weighted CN, CN2=DA3 post weighted CN Correct (tr, (tr, (tr, (min.)) Travel CN1 91 2.67 242.97 1 Land Length Roughness Slope Time, Travel CN4 0.00 CN3 0.00 S Image: Consposite CN = 01 Image: Consposite CN = 01 Image: CN = 01 S </td <td></td> <td>CN₅</td> <td></td> <td></td> <td>0.00</td> <td>l</td> <td>5</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> | | CN ₅ | | | 0.00 | l | 5 | | | | | | | | |
| Composite CN = 77 Total Time of Concentration, T _c (min.) 8.6 Runoff 1 Yr. 10 Yr. 100 Yr. 77 < | Undetained | Total | - | 1.32 | 101.20 | l | 6 | Other Tt | | | | | 8.6 | | |
| Composite CN Tr TO Tr Tr Storage (in.) S=1000/CN-10 2.99 2.99 2.99 10114 abstration (in.), 1, e0.25 0.60 0.60 0.60 0.60 Runoff depth (in.), 0, e(P-0.2S) ² /((P1,)+S) 0.59 1.86 3.87 Hydrograph No.: Contributes to 21 Notes: See "The Farm" calcs by others. CN1=DA1 post weighted CN, CN2=DA3 post weighted CN Hydrograph No.: Contributes to 21 Notes: See "The Farm" calcs by others. CN1=DA1 post weighted CN, CN2=DA3 post weighted CN Hydrograph No.: Contributes to 21 Notes: See "The Farm" calcs by others. CN1=DA1 post weighted CN, CN2=DA3 post weighted CN Hydrograph No.: Contributes to 21 Notes: Composite Curve Number (CN) Time of Concentration, Tc Travel Flow Land Length Rungthess Slope Travel CN Area (Ac.) CN*A 0.00 3 Land Length Rungthess Slope Travel GNA 0.000 CN 2 Land Land Land Land Land Land Land | areas total | | Co | mposite CN = | 77 | l | | | Total Tim | ne of Con | centration, T | _c (min.) | 8.6 | | |
| Runoff I Yr. 10 Yr. 77 77 Storage (m.) S=1000/CN-10 2.99 2.99 2.99 2.99 2.99 2.99 2.99 2.99 2.99 2.99 2.99 2.99 2.99 2.99 100 Yr. Provide Colspan="2">Provide Colspan="2">Provide Colspan="2" Provide Colspan="2" Provide Colspan="2" <th <="" colspan="2" t<="" td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th> | <td></td> | | | | | | | | | | | | | | |
| Composite CN 17 77 77 Storage (in.) S=1000/CN-10 2.99 2.99 2.99 2.99 Initial abstraction (in.), I ₂ =0.25 0.60 0.60 0.60 Runoff depth (in.), Q=(P-0.2S) ⁷ /([P-I ₂)+S] 0.59 1.86 3.87 Runoff volume (ac-ft), RV = Q/12*A 0.07 0.20 0.43 Flow rate (cfs), q _{peak} from hydrograph 1.20 3.89 Hydrograph No.: Contributes to 21 Notes: See "The Farm" calcs by others. CN1=DA1 post weighted CN, CN2=DA3 post weighted CN Flow Regime Contributes to 21 Notes: See "The Farm" calcs by others. CN1=DA1 post weighted CN, CN2=DA3 post weighted CN Travel CN1 91 2.67 242.97 Land Length Roughness Slope Time, T, Segment Flow Regime Cover I Image: Cover (ft) Coeff., n (ft/ft) Image: Cover Image: Cover (ft) Coeff., n (ft/ft) Image: Cover (ft) Image: Cover (ft) <td></td> <td> </td> <td></td> <td></td> <td>Runoff</td> <td>1 Vr</td> <td>10 Vr</td> <td>100 Vr</td> <td>4</td> <td></td> <td></td> <td></td> <td></td> | | | | | Runoff | 1 Vr | 10 Vr | 100 Vr | 4 | | | | | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | Com | nacita CN | | 1 Yr. | 10 Yr. | 100 Yr. | - | | | | | | |
| Composite Curve Number (CN) L.33 L.33 <thlist andis="" for="" in="" int<="" inter="" interval="" td="" the=""><td></td><td>Str</td><td>unage (in</td><td>VS=1000/CN-</td><td>10</td><td>2 99</td><td>2 99</td><td>2.99</td><td>-</td><td></td><td></td><td></td><td></td></thlist> | | Str | unage (in | VS=1000/CN- | 10 | 2 99 | 2 99 | 2.99 | - | | | | | | |
| Initial additional (in,), q=0.22)?/[[P-l_a],*5] 0.50 0.50 0.50 Runoff depth (in,), q=(P-0.25)?/[[P-l_a],*5] 0.59 1.86 3.87 Runoff volume (ac-ft), R v = 0/12*A 0.07 0.20 0.43 Flow rate (cfs), q _{peak} from hydrograph 1.20 3.89 Hydrograph No.: Contributes to 21 Notes: See "The Farm" calcs by others. CN1=DA1 post weighted CN, CN2=DA3 post weighted CN Hydrograph No.: Contributes to 21 Notes: See "The Farm" calcs by others. CN1=DA1 post weighted CN, CN2=DA3 post weighted CN Hydrograph No.: Contributes to 21 Notes: See "The Farm" calcs by others. CN1=DA1 post weighted CN, CN2=DA3 post weighted CN Hydrograph No.: Contributes to 21 Composite Curve Number (CN) Time of Concentration, Te Travel Travel CN1 91 2.67 242.97 1 Land Length Roughness Slope Time, Tr CN2 0.000 0.4 0.00 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | | al abstra | $\frac{1}{1}$ $\frac{1}{1}$ $\frac{1}{1}$ $\frac{1}{1}$ $\frac{1}{1}$ | 1.25 | 0.60 | 0.60 | 0.60 | - | | | | | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | Bupoff de | anth (in) | $\frac{1}{10000000000000000000000000000000000$ | ۰.25 [/۲.۱.۱۰۶] | 0.00 | 1 06 | 2 07 | - | | | | | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | $\frac{1}{(200 \text{ ft})}$ $\frac{1}{(200 \text{ ft})}$ $\frac{1}{(200 \text{ ft})}$ $\frac{1}{(200 \text{ ft})}$ | (P-1a)+3] | 0.35 | 0.20 | 0.42 | - | | | | | | |
| Indef rate (bis), dpeak from hydrograph 1.20 3.32 inversion of the second s | | Elow rat | Volume | $\frac{(ac-ii)}{c}$, $\pi v = u$ | /12 [·] A | 1.20 | 2.89 | 0.45 | | nh No · | Contributes | +- 21 | | | |
| Area to "The Farm" detention Composite Curve Number (CN) Time of Concentration, T _c Travel Time, T _t CN Area (Ac.) CN*A Flow Land Length Roughness Slope Travel CN1 91 2.67 242.97 CN Cover (ft) Coeff., n (ft/ft) (min.) CN3 0.00 3 0.00 3 0.00 3 0.00 1 0 0 0 0 CN4 0.000 CN5 0.000 3 0.00 3 0 | | Notec | | Ipeak ITOITTIYUT | by others CN | 1-DA1 post | s.os | | | рн мо см | Contributes | | | | |
| Time of Concentration, T _c Composite Curve Number (CN) Time of Concentration, T _c CN Area (Ac.) CN*A CN1 91 2.67 242.97 CN2 0.00 2 0 0 CN3 0.00 3 0 0 CN4 0.00 3 0 0 0 CN3 0.00 3 0 0 0 0 CN4 0.00 0 3 0 0 0 0 CN3 0.00 0 4 0 <t< td=""><td></td><td>INDIES.</td><td>See in</td><td></td><td>by others. Civ.</td><td>1-DAT 0031</td><td>Weighted C</td><td>N, CN2-DA3 p03</td><td>I Weighten</td><td>_11</td><td></td><td></td><td></td></t<> | | INDIES. | See in | | by others. Civ. | 1-DAT 0031 | Weighted C | N, CN2-DA3 p03 | I Weighten | _11 | | | | | |
| Kea to "The Farm" detention Composite CN = 91 Segment Flow Regime Land Length Cover Roughness Cover Slope Time, Ti | | Com | posite C | urve Number (| (CN) | | 1 | | Time of Con | centratio | n, T _c | | | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | ļ , | | 1 | | | | | | | Travel | | |
| $ \begin{array}{ c c c c c c } \hline CN & Area (Ac.) & CN*A \\ \hline CN_1 & 91 & 2.67 & 242.97 \\ \hline CN_2 & 0 & 0.00 \\ \hline CN_2 & 0 & 0.00 \\ \hline CN_3 & 0 & 0.00 \\ \hline CN_4 & 0 & 0.00 \\ \hline CN_5 & 0 & 0.00 \\ \hline Total & - & 2.67 & 242.97 \\ \hline Total & - & 2.67 & 242.97 \\ \hline \hline Composite CN = & 91 \\ \hline $ | | | | | | l | Flow | | Land | Length | Roughness | Slope | Time, T _t | | |
| $ \begin{array}{c c c c c c c c c c c c c c c c c c c $ | | | CN | Area (Ac.) | CN*A | 1 | Segment | Flow Regime | Cover | (ft) | Coeff., n | (ft/ft) | (min.) | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | CN ₁ | 91 | 2.67 | 242.97 | 1 | 1 | | | | | | | | |
| CN_3 0.00 CN_4 0.00 CN_5 0.00 CN_5 0.00 $Total$ - 2.67 242.97 G G G G G G $Total$ - 2.67 242.97 G G G G G $Composite CN = 91$ G | | CN ₂ | | | 0.00 | 1 | 2 | | | | | | | | |
| Area to "The Farm" detention CN_4 0.00 CN_5 0.00 $Total$ - 2.67 242.97 G $Other Tt$ G G $Composite CN = 91$ G G G $Composite CN = 91$ G G G G $Composite CN = 91$ G G G G G $Composite CN = 91$ G G G G G G $VRRM CN^*$ 91 91 91 91 91 91 S $Storage (in.) S=1000/CN-10$ 0.99 0.99 0.99 0.99 $BMPs$ are utilized $Initial abstraction (in.), I_a=0.25$ 0.20 0.20 0.20 0.20 0.20 $Runoff depth (in.), Q=(P-0.2S)^2/[(P-I_a)+S]$ 1.39 3.07 5.39 Sag $Hydrograph$ No.: 19 $Hydrograph No.: 19 13.12 19 10 10 10 $ | | CN ₃ | | | 0.00 | l | 3 | | | | | | | | |
| Area to "The Farm" detention CN_5 0.005 d d d Total-2.67242.976Other Tt5.8Composite CN = 91Total Time of Concentration, T _c (min.)5.8Total Time of Concentration, T _c (min.)5.8VRRM CN*919191*If different from Composite CN, runoff reductionStorage (in.) S=1000/CN-100.990.990.99Initial abstraction (in.), I _a =0.2S0.200.200.20BMPs are utilizedRunoff depth (in.), Q=(P-0.2S) ² /[(P-I _a)+S]1.393.075.39Hydrograph No.:19Notes:See "The Earm" calcs by others:0.11=DA3 post weighted CNHydrograph No.:19 | | CN ₄ | | | 0.00 | l | 4 | | | | | | | | |
| Area to "The Farm" detention Total - 2.67 242.97 6 Other Tt Image: Composite CN = 91 5.8 Gomposite CN = 91 Total Time of Concentration, T _c (min.) 5.8 Total Time of Concentration, T _c (min.) 5.8 Total Time of Concentration, T _c (min.) 5.8 Runoff VRRM CN* 91 91 91 91 91 Storage (in.) S=1000/CN-10 0.99 0.99 0.99 0.99 BMPs are utilized Initial abstraction (in.), l _a =0.2S 0.20 0.20 0.20 0.20 0.20 0.20 BMPs are utilized Hydrograph Hydrograph Hydrograph Hydrograph 19 Hydrograph No.: 19 19 Hydrograph No.: 19 10 Hydrograph No.: 19 10 Hydrograph No.: 19 Hydrograph No.: 19 Hydrograph No.: 19 10 Hydrograph No.: 19 10 Hydrograph No. | | CN ₅ | | | 0.00 | 1 | 5 | | | | | | | | |
| Total Time of Concentration, T_c (min.)5.8Farm" detentionTotal Time of Concentration, T_c (min.)5.8RunoffVRRM CN*919191Storage (in.) S=1000/CN-100.990.990.99Initial abstraction (in.), I_a =0.2S0.200.200.20Runoff depth (in.), Q=(P-0.2S) ² /[(P-I_a)+S]1.393.075.39Runoff volume (ac-ft), RV = Q/12*A0.310.681.20Hydrograph No.:191919Notes:See "The Earm" calcs by others: CN1=DA3 post weighted CNNotes: | Area to "The | Total | <u> </u> | 2.67 | 242.97 | l | 6 | Other Tt | | | | | 5.8 | | |
| Runoff *If different from Composite CN, runoff reduction VRRM CN* 91 91 91 Storage (in.) S=1000/CN-10 0.99 0.99 0.99 BMPs are utilized Initial abstraction (in.), I_a =0.25 0.20 0.20 0.20 BMPs are utilized Runoff depth (in.), Q=(P-0.2S) ² /[(P-I_a)+S] 1.39 3.07 5.39 5.39 Runoff volume (ac-ft), RV = Q/12*A 0.31 0.68 1.20 Hydrograph No.: 19 | Farm" detention | | Co | mposite CN = | 91 | | | | Total Tim | ne of Con | centration, T | _շ (min.) | 5.8 | | |
| Runoff I Yr. 100 Yr. VRRM CN* 91 91 91 Storage (in.) S=1000/CN-10 0.99 0.99 0.99 0.99 Initial abstraction (in.), I _a =0.2S 0.20 0.20 0.20 0.20 Runoff depth (in.), Q=(P-0.2S) ² /[(P-I _a)+S] 1.39 3.07 5.39 BMPs are utilized Runoff volume (ac-ft), RV = Q/12*A 0.31 0.68 1.20 Hydrograph No.: 19 | | | | | | | | | | | | | | | |
| Image: Non-state of the state of the s | | | | | Runoff | 1 Vr | 10 Vr | 100.1/2 | _ | | | | | | |
| Storage (in.) S=1000/CN-10 0.99 0.99 0.99 0.99 BMPs are utilized Initial abstraction (in.), I_a =0.2S 0.20 0.20 0.20 1.39 3.07 5.39 Runoff depth (in.), Q=(P-0.2S) ² /[(P-I_a)+S] 1.39 3.07 5.39 1.20 Hydrograph No.: 19 Notes: See "The Farm" cales by others: CN1=DA3 post weighted CN See "The Farm" cales by others: CN1=DA3 post weighted CN Hydrograph No.: 19 | | | | | | | <u>10 11.</u> | 91 | +If differen | at from C | amposita CN | rupoff | roduction | | |
| Initial abstraction (in.), I _a =0.2S 0.20 0.20 0.20 Runoff depth (in.), Q=(P-0.2S) ² /[(P-I _a)+S] 1.39 3.07 5.39 Runoff volume (ac-ft), RV = Q/12*A 0.31 0.68 1.20 Flow rate (cfs), q _{peak} from hydrograph 6.19 13.12 Hydrograph No.: 19 | | Str | | 1 S=1000/CN- | 10 | 0.00 | 0 00 | 0.99 | | It II UIII C | omposite Civ, | , runon | reduction | | |
| Runoff depth (in.), Q=(P-0.2S) ² /[(P-I _a)+S] 1.39 3.07 5.39 Runoff volume (ac-ft), RV = Q/12*A 0.31 0.68 1.20 Flow rate (cfs), q _{peak} from hydrograph 6.19 13.12 Hydrograph No.: 19 | | | al abstra | $\frac{1}{1000}$ (in) 1 =(| 1 25 | 0.55 | 0.55 | 0.55 | | utinzeu | | | | | |
| Ruhom depth (in.), $Q = (P - 0.2S) / [(P - l_a) + S]$ 1.393.075.39Runoff volume (ac-ft), RV = Q/12*A0.310.681.20Flow rate (cfs), q_{peak} from hydrograph6.1913.12Hydrograph No.:19Notes:See "The Farm" calcs by othersCN1=DA3 post weighted CN19 | | | | $\frac{1}{2}$ | ······································ | 1 20 | 2.07 | 5.20 | - | | | | | | |
| Runom volume (ac-m), RV = Q/12*A 0.31 0.08 1.20 Flow rate (cfs), q _{peak} from hydrograph 6.19 13.12 Hydrograph No.: 19 Notes: See "The Farm" calcs by others: CN1=DA3 post weighted CN | | Runon ue | ptn (m.) | , Q=(P-0.25) / [| $[(P-I_a)+S]$ | 1.39 | 3.07 | 5.39 | _ | | | | | | |
| Plow rate (cis), q _{peak} iron iron ographication in the second se | | Elow rat | Volume | $\frac{(ac-ii)}{c}$, $\pi v = Q$ | /12 [·] A | 6.10 | 12 12 | 1.20 | | sob No · | 10 | | | | |
| | | Notes | See "Th | Peak ITOITTIYUT | by others CN | 1=D43 post | uveighted (| `N | | ipii No | | | | | |

Drainage Area Runoff and Time of Concentration

Drainage Area: Undetained Farm and other contrib. offsite flows PRE & POST

| Composite Curve Number (CN) | | | | | | Notes: |
|-----------------------------|-----------------|--------------------|----|---------------|--------|---------------------------------|
| | Hydrologic Soil | | | | | |
| | Group | Land Cover | CN | Area, A (ac.) | CN*A | |
| CN_1 | N/A | "Farm" DA1 post CN | 79 | 0.55 | 43.45 | -CN1 and CN2 are pulled from |
| CN ₂ | N/A | "Farm" DA3 post CN | 75 | 0.77 | 57.75 | "The Farm" SWM plan. "The |
| CN ₃ | D | Imperv. | 98 | 1.25 | 122.30 | Farm" DA1 and DA3 are |
| CN ₄ | D | Open space | 80 | 0.72 | 57.59 | undetained by the |
| CN ₅ | D | Brush (good) | 73 | 1.53 | 111.33 | development. DA2 is |
| CN ₆ | С | Imperv. | 98 | 0.28 | 27.15 | routed through "The Farm's" |
| CN ₇ | | | | | 0.00 | SWM improvements. |
| CN ₈ | | | | | 0.00 | -Remaining CNs are measured |
| CN ₉ | | | | | 0.00 | areas from offsite areas, incl. |
| CN ₁₀ | | | | | 0.00 | 460 and its median. |
| Total 5.09 | | | | | 419.57 | |
| Composite CN = | | | | | 82 | |

| Time of Concentration, T _c | | | | | | | |
|---------------------------------------|----------------------------|------------|--------------|----------------|-------------------------|-----------------------------|--|
| | 2 yr. Precip. (in.) = 2.73 | | | | | | |
| | | | | Roughness | Slope | Travel Time, T _t | |
| Flow Segment | Flow Regime | Land Cover | Length (ft) | Coeff., n | (ft/ft) | (min.) | |
| 1 | Other Tt | Farm Tc | | | | 8.6 | |
| 2 | | | | | | | |
| 3 | | | | | | | |
| 4 | | | | | | | |
| 5 | | | | | | | |
| 6 | | | | | | | |
| 7 | | | | | | | |
| 8 | | | | | | | |
| 9 | | | | | | | |
| 10 | | | | | | | |
| | | Tota | l Time of Co | ncentration, 1 | Γ _c (min.) = | 8.6 | |

| Runoff | | | | | | | |
|--|-------|--------|---------|--|--|--|--|
| | 1 Yr. | 10 Yr. | 100 Yr. | | | | |
| Precipitation (in.), P | 2.26 | 4.06 | 6.44 | | | | |
| Composite CN | 82 | 82 | 82 | | | | |
| Storage (in.) S=1000/CN-10 | 2.20 | 2.20 | 2.20 | | | | |
| Initial abstraction (in.), I _a =0.2S | 0.44 | 0.44 | 0.44 | | | | |
| Runoff depth (in.), Q=(P-0.2S) ² /[(P-I _a)+S] | 0.83 | 2.25 | 4.39 | | | | |
| Runoff volume (ac-ft), RV = Q/12*A | 0.35 | 0.96 | 1.86 | | | | |
| Flow rate (cfs), q _{peak} from hydrograph | 6.64 | 18.18 | 34.74 | | | | |
| Hydrograph Number: | 21 | | | | | | |

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Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 21

Undet. Farm and other contrib. offsite

| Hydrograph type | = SCS Runoff | Peak discharge | = 6.643 cfs |
|-----------------|--------------|--------------------|---------------|
| Storm frequency | = 1 yrs | Time to peak | = 720 min |
| Time interval | = 2 min | Hyd. volume | = 15,256 cuft |
| Drainage area | = 5.090 ac | Curve number | = 82 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 8.60 min |
| Total precip. | = 2.26 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 21

Undet. Farm and other contrib. offsite

| Hydrograph type | = SCS Runoff | Peak discharge | = 18.18 cfs |
|-----------------|--------------|--------------------|---------------|
| Storm frequency | = 10 yrs | Time to peak | = 718 min |
| Time interval | = 2 min | Hyd. volume | = 41,653 cuft |
| Drainage area | = 5.090 ac | Curve number | = 82 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 8.60 min |
| Total precip. | = 4.06 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 22

Total Offsite thru Southern Reach

| Hydrograph type Storm frequency | = Combine = 1 vrs | Peak discharge Time to peak | = 46.84 cfs = 720 min |
|------------------------------------|----------------------|--------------------------------|--------------------------|
| Time interval | = 2 min | Hyd. volume | = 144,746 cuft |
| Inflow hyds. | = 18, 20, 21 | Contrib. drain. area | = 5.090 ac |



Tuesday, 11 / 1 / 2022

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 22

Total Offsite thru Southern Reach

| Hydrograph type Storm frequency | = Combine = 10 vrs | Peak discharge Time to peak | = 86.16 cfs = 720 min |
|------------------------------------|-----------------------|--------------------------------|--------------------------|
| Time interval | $= 2 \min$ | Hyd. volume | = 341,950 cuft |
| Inflow hyds. | = 18, 20, 21 | Contrib. drain. area | = 5.090 ac |



Tuesday, 11 / 1 / 2022





Drainage Area Runoff and Time of Concentration

Drainage Area: PRE OTHER AREA CONTRIB. AT CONFLUENCE PREDEVELOPMENT

| Composite Curve Number (CN) | | | | | | Notes: |
|-----------------------------|-----------------|--------------------|----|---------------|---------|------------------------------------|
| | Hydrologic Soil | | | | | |
| | Group | Land Cover | CN | Area, A (ac.) | CN*A | |
| CN1 | В | Open space | 61 | 16.39 | 999.91 | |
| CN ₂ | C | Open space | 74 | 12.04 | 890.69 | |
| CN ₃ | В | Imperv. (measured) | 98 | 0.00 | 0.00 | "Other area" contributing at |
| CN ₄ | C | Imperv. (measured) | 98 | 0.00 | 0.00 | the confluence of the north |
| CN ₅ | В | Woods (good) | 55 | 0.00 | 0.00 | and south channels. Comprises |
| CN ₆ | С | Woods (good) | 70 | 0.00 | 0.00 | onsite and offsite areas |
| CN ₇ | | | | | 0.00 | downstream from detention |
| CN ₈ | | | | | 0.00 | measures. |
| CN ₉ | | | | | 0.00 | |
| CN ₁₀ | | | | | 0.00 | |
| Total 28.43 | | | | | 1890.59 |] |
| | | | Со | mposite CN = | 67 | |

| Time of Concentration, T _c | | | | | | |
|---------------------------------------|---------------|------------|--------------|----------------|-------------------------|-----------------------------|
| 2 yr. Precip. (in.) = 2.73 | | | | | | |
| | | | | Roughness | Slope | Travel Time, T _t |
| Flow Segment | Flow Regime | Land Cover | Length (ft) | Coeff., n | (ft/ft) | (min.) |
| 1 | Sheet Flow | Grass | 100 | 0.24 | 0.05 | 10.7 |
| 2 | Shallow Conc. | Grass | 1100 | | 0.091 | 3.8 |
| 3 | | | | | | |
| 4 | | | | | | |
| 5 | | | | | | |
| 6 | | | | | | |
| 7 | | | | | | |
| 8 | | | | | | |
| 9 | | | | | | |
| 10 | | | | | | |
| | | Tota | l Time of Co | ncentration, 1 | 「 _c (min.) = | 14.5 |

| Runoff | | | | | | | |
|--|-------|--------|---------|--|--|--|--|
| | 1 Yr. | 10 Yr. | 100 Yr. | | | | |
| Precipitation (in.), P | 2.26 | 4.06 | 6.44 | | | | |
| Composite CN | 67 | 67 | 67 | | | | |
| Storage (in.) S=1000/CN-10 | 4.93 | 4.93 | 4.93 | | | | |
| Initial abstraction (in.), I _a =0.2S | 0.99 | 0.99 | 0.99 | | | | |
| Runoff depth (in.), Q=(P-0.2S) ² /[(P-I _a)+S] | 0.26 | 1.18 | 2.87 | | | | |
| Runoff volume (ac-ft), RV = Q/12*A | 0.62 | 2.80 | 6.79 | | | | |
| Flow rate (cfs), q _{peak} from hydrograph | 5.61 | 39.92 | 102.14 | | | | |
| Hydrograph Number: | 26 | | | | | | |

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Wednesday, 11 / 2 / 2022

Hyd. No. 26

PRE OTHER AREA CONTRIB. AT CONFLUENCE

| Hydrograph type = | SCS Runoff | Peak discharge | = 5.612 cfs |
|-------------------|-------------|--------------------|---------------|
| Storm frequency = | = 1 yrs | Time to peak | = 12.10 hrs |
| Time interval = | = 2 min | Hyd. volume | = 26,375 cuft |
| Drainage area = | = 28.430 ac | Curve number | = 67 |
| Basin Slope = | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method = | = User | Time of conc. (Tc) | = 14.50 min |
| Total precip. = | = 2.26 in | Distribution | = Type II |
| Storm duration = | = 24 hrs | Shape factor | = 484 |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Wednesday, 11 / 2 / 2022

Hyd. No. 26

PRE OTHER AREA CONTRIB. AT CONFLUENCE

| Hydrograph type | = SCS Runoff | Peak discharge | = 39.92 cfs |
|-----------------|--------------|--------------------|----------------|
| Storm frequency | = 10 yrs | Time to peak | = 12.07 hrs |
| Time interval | = 2 min | Hyd. volume | = 118,919 cuft |
| Drainage area | = 28.430 ac | Curve number | = 67 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 14.50 min |
| Total precip. | = 4.06 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 28

Ex. TOB Pond outfall routed to confluence

| Hydrograph type = Storm frequency = | Reach 1 vrs | Peak discharge Time to peak | = 27.06 cfs = 742 min |
|--|-----------------------------|--------------------------------|--------------------------|
| Time interval = | 2 min | Hyd. volume | = 231,957 cuft |
| Inflow hyd. No. = | 11 - Predev Ex.TOB Pond Out | Section type | = Triangular |
| Reach length = | = 436.0 ft | Channel slope | = 2.0 % |
| Manning's n = | 0.030 | Bottom width | = 0.0 ft |
| Side slope = | 3.0:1 | Max. depth | = 0.0 ft |
| Rating curve x = | 3.074 | Rating curve m | = 1.333 |
| Ave. velocity = | = 0.00 ft/s | Routing coeff. | = 0.9855 |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 28

Ex. TOB Pond outfall routed to confluence

| Hydrograph type | = Reach | Peak discharge | = 35.75 cfs |
|-----------------|-------------------------------|----------------|----------------|
| Storm frequency | = 10 yrs | Пте то реак | = 754 min |
| l ime interval | = 2 min | Hyd. volume | = 661,722 cuft |
| Inflow hyd. No. | = 11 - Predev Ex.TOB Pond Out | tSection type | = Triangular |
| Reach length | = 436.0 ft | Channel slope | = 2.0 % |
| Manning's n | = 0.030 | Bottom width | = 0.0 ft |
| Side slope | = 3.0:1 | Max. depth | = 0.0 ft |
| Rating curve x | = 3.074 | Rating curve m | = 1.333 |
| Ave. velocity | = 0.00 ft/s | Routing coeff. | = 1.0203 |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 29

South Offsite Routed to Confluence

| Hydrograph type Storm frequency | = Reach = 1 yrs | Peak discharge Time to peak | = 45.94 cfs = 722 min |
|---------------------------------|-----------------------------------|--------------------------------|--------------------------|
| Time interval | = 2 min | Hyd. volume | = 144,743 cuft |
| Inflow hyd. No. | = 22 - Total Offsite thru Souther | r SRetioh type | = Triangular |
| Reach length : | = 877.0 ft | Channel slope | = 2.3 % |
| Manning's n | = 0.030 | Bottom width | = 0.0 ft |
| Side slope : | = 3.0:1 | Max. depth | = 0.0 ft |
| Rating curve x | = 3.296 | Rating curve m | = 1.333 |
| Ave. velocity | = 6.40 ft/s | Routing coeff. | = 0.7372 |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 29

South Offsite Routed to Confluence

| Hydrograph type=Storm frequency=Time interval=Inflow hyd. No.=Reach length=Manning's p= | = Reach | Peak discharge | = 85.44 cfs |
|---|-----------------------------------|------------------------|----------------|
| | = 10 yrs | Time to peak | = 722 min |
| | = 2 min | Hyd. volume | = 341,946 cuft |
| | = 22 - Total Offsite thru Souther | r Steetich type | = Triangular |
| | = 877.0 ft | Channel slope | = 2.3 % |
| | = 0.030 | Bottom width | = 0.0 ft |
| Reach length=Manning's n=Side slope=Rating curve x= | = 877.0 ft | Channel slope | = 2.3 % |
| | = 0.030 | Bottom width | = 0.0 ft |
| | = 3.0:1 | Max. depth | = 0.0 ft |
| | = 3.296 | Rating curve m | = 1.333 |
| Ave. velocity | = 7.45 ft/s | Routing coeff. | = 0.8094 |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Tuesday, 11 / 1 / 2022

Hyd. No. 30

PRE COMBINED AT CONFLUENCE

| Hydrograph type Storm frequency | = Combine = 1 vrs | Peak discharge Time to peak | = 73.96 cfs = 724 min |
|------------------------------------|----------------------|--------------------------------|--------------------------|
| Time interval | = 2 min | Hyd. volume | = 403,075 cuft |
| Inflow hyds. | = 26, 28, 29 | Contrib. drain. area | = 28.430 ac |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 30

PRE COMBINED AT CONFLUENCE

| Hydrograph type= CombinePeak discharge= 154.45 clsStorm frequency= 10 yrsTime to peak= 724 minTime interval= 2 minHyd. volume= 1,122,588 cuftInflow hyds.= 26, 28, 29Contrib. drain. area= 28.430 ac | Hydrograph type | = Combine | Peak discharge | = 154.45 cfs |
|--|-----------------|--------------|----------------------|------------------|
| | Storm frequency | = 10 yrs | Time to peak | = 724 min |
| | Time interval | = 2 min | Hyd. volume | = 1,122,588 cuft |
| | Inflow hyds. | = 26, 28, 29 | Contrib. drain. area | = 28.430 ac |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 31

COMBINED ROUTED TO PROPERTY LINE

| Hydrograph type Storm frequency | = Reach = 1 vrs | Peak discharge Time to peak | = 73.47 cfs = 726 min |
|------------------------------------|----------------------------|--------------------------------|--------------------------|
| Time interval | = 2 min | Hyd. volume | = 403,072 cuft |
| Inflow hyd. No. | = 30 - PRE COMBINED AT COM | A Steddie N C/Ee | = Triangular |
| Reach length | = 775.0 ft | Channel slope | = 2.0 % |
| Manning's n | = 0.030 | Bottom width | = 0.0 ft |
| Side slope | = 3.0:1 | Max. depth | = 0.0 ft |
| Rating curve x | = 3.074 | Rating curve m | = 1.333 |
| Ave. velocity | = 6.81 ft/s | Routing coeff. | = 0.8254 |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 31

COMBINED ROUTED TO PROPERTY LINE

| Hydrograph type Storm frequency | = Reach = 10 yrs | Peak discharge Time to peak | = 154.33 cfs = 726 min |
|------------------------------------|----------------------------|--------------------------------|---------------------------|
| Time interval | = 2 min | Hyd. volume | = 1,122,586 cuft |
| Inflow hyd. No. | = 30 - PRE COMBINED AT COI | NSFeddtiEIN Cylipe | = Triangular |
| Reach length | = 775.0 ft | Channel slope | = 2.0 % |
| Manning's n | = 0.030 | Bottom width | = 0.0 ft |
| Side slope | = 3.0:1 | Max. depth | = 0.0 ft |
| Rating curve x | = 3.074 | Rating curve m | = 1.333 |
| Ave. velocity | = 8.18 ft/s | Routing coeff. | = 0.9158 |



Drainage Area Runoff and Time of Concentration

Drainage Area: PRE OTHER AREA CONTRIB. AT POA PREDEVELOPMENT

| - | Composite Curve Number (CN) | | | | | Notes: |
|------------------|-----------------------------|--------------------|-------|---------------|---------|------------------------------|
| | Hydrologic Soil | | | | | |
| | Group | Land Cover | CN | Area, A (ac.) | CN*A | |
| CN ₁ | В | Open space | 61 | 8.08 | 492.75 | |
| CN ₂ | С | Open space | 74 | 2.84 | 210.02 | |
| CN ₃ | В | Imperv. (measured) | 98 | 0.00 | 0.00 | |
| CN ₄ | С | Imperv. (measured) | 98 | | 0.00 | "Other area" contributing to |
| CN ₅ | В | Woods (good) | 55 | 2.34 | 128.48 | the point of analysis. |
| CN ₆ | C | Woods (good) | 70 | 4.89 | 342.25 | areas downstream from |
| CN ₇ | | | | | 0.00 | detention measures. |
| CN ₈ | | | | | 0.00 | |
| CN ₉ | | | | | 0.00 | |
| CN ₁₀ | | | | | 0.00 | |
| | | | Total | 18.14 | 1173.50 | |
| | | | Со | mposite CN = | 65 | |

| Time of Concentration, T _c | | | | | | |
|--|----------------------------|------------|-------------|-----------|---------|-----------------------------|
| | 2 yr. Precip. (in.) = 2.73 | | | | | |
| | | | | Roughness | Slope | Travel Time, T _t |
| Flow Segment | Flow Regime | Land Cover | Length (ft) | Coeff., n | (ft/ft) | (min.) |
| 1 | Sheet Flow | Grass | 100 | 0.24 | 0.05 | 10.7 |
| 2 | Shallow Conc. | Grass | 1100 | | 0.091 | 3.8 |
| 3 | Channel | Grass | 834 | 0.03 | 0.019 | 3.7 |
| 4 | | | | | | |
| 5 | | | | | | |
| 6 | | | | | | |
| 7 | | | | | | |
| 8 | | | | | | |
| 9 | | | | | | |
| 10 | | | | | | |
| Total Time of Concentration, T _c (min.) = | | | | | 18.2 | |

| Runoff | | | | | | | |
|--|-------|--------|---------|--|--|--|--|
| | 1 Yr. | 10 Yr. | 100 Yr. | | | | |
| Precipitation (in.), P | 2.26 | 4.06 | 6.44 | | | | |
| Composite CN | 65 | 65 | 65 | | | | |
| Storage (in.) S=1000/CN-10 | 5.38 | 5.38 | 5.38 | | | | |
| Initial abstraction (in.), I _a =0.2S | 1.08 | 1.08 | 1.08 | | | | |
| Runoff depth (in.), Q=(P-0.2S) ² /[(P-I _a)+S] | 0.21 | 1.06 | 2.68 | | | | |
| Runoff volume (ac-ft), RV = Q/12*A | 0.32 | 1.61 | 4.05 | | | | |
| Flow rate (cfs), q _{peak} from hydrograph | 2.10 | 20.29 | 55.29 | | | | |
| Hydrograph Number: | 27 | | | | | | |

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Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 27

PRE OTHER AREA CONTRIB. AT POA

| Hydrograph type | = SCS Runoff | Peak discharge | = 2.100 cfs |
|-----------------|--------------|--------------------|---------------|
| Storm frequency | = 1 yrs | Time to peak | = 728 min |
| Time interval | = 2 min | Hyd. volume | = 14,030 cuft |
| Drainage area | = 18.140 ac | Curve number | = 65 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 18.20 min |
| Total precip. | = 2.26 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 27

PRE OTHER AREA CONTRIB. AT POA

| Hydrograph type | = SCS Runoff | Peak discharge | = 20.29 cfs |
|-----------------|--------------|--------------------|---------------|
| Storm frequency | = 10 yrs | Time to peak | = 726 min |
| Time interval | = 2 min | Hyd. volume | = 70,027 cuft |
| Drainage area | = 18.140 ac | Curve number | = 65 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 18.20 min |
| Total precip. | = 4.06 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



Drainage Area Runoff and Time of Concentration

| Precipitation Data | | | | | |
|--------------------|---------|--|--|--|--|
| Return | | | | | |
| Frequency | P (in.) | | | | |
| 1 Yr. | 2.26 | | | | |
| 2 Yr. | 2.73 | | | | |
| 10 Yr. | 4.06 | | | | |
| 100 Yr. | 6.44 | | | | |

| Drainage Area: | To Village Pha | ase 1 Por | nd | | | | | | | | | |
|----------------|-----------------|-------------|---------------------------------|-------------------------|------------|---------------------------|---------------|--|-----------|-------------------|---------|----------------------|
| | Com | posite C | urve Number (| (CN) |] | | ٦ | ime of Con | centratio | n, T _c | | |
| | | | | | | | | | | | | Travel |
| | | | | | | Flow | | Land | Length | Roughness | Slope | Time, T _t |
| | | CN | Area (Ac.) | CN*A | | Segment | Flow Regime | Cover | (ft) | Coeff., n | (ft/ft) | (min.) |
| | CN ₁ | 75 | 8.20 | 615.26 | | 1 | Sheet Flow | Grass | 100 | 0.24 | 0.087 | 8.6 |
| | CN ₂ | | | 0.00 | | 2 | Shallow Conc. | Unpaved | 120 | | 0.16 | 0.3 |
| | CN ₃ | | | 0.00 | | 3 | Channel | Grass | 478 | 0.03 | 0.042 | 1.7 |
| | CN ₄ | | | 0.00 | | 4 | | | | | | |
| | CN ₅ | | | 0.00 | | 5 | | | | | | |
| | Total | - | 8.20 | 615.26 | | 6 | | | | | | |
| Predev. | | Co | omposite CN = | 75 | | | | Total Time of Concentration, T _c (min.) | | | 10.6 | |
| | | | | | | | | | | | | • |
| | | | | Runoff | - | - | | | | | | |
| | | | | | 1 Yr. | 10 Yr. | 100 Yr. | | | | | |
| | | Com | posite CN | | 75 | 75 | 75 | | | | | |
| | St | orage (in | .) S=1000/CN-1 | 10 | 3.33 | 3.33 | 3.33 | | | | | |
| | Init | al abstra | iction (in.), I _a =0 | .25 | 0.67 | 0.67 | 0.67 | | | | | |
| | Runoff d | epth (in.) |), Q=(P-0.2S) ² / | [(P-I _a)+S] | 0.52 | 1.71 | 3.66 | | | | | |
| | Runof | f volume | (ac-ft), RV = Q | /12*A | 0.35 | 1.17 | 2.50 | | | | | |
| | Flow ra | te (cfs), d | q _{peak} from hydr | ograph | 5.51 | 20.07 | | Hydrogra | ph No.: | 24 | | |
| | | | | 75 | CNI from) | m Village Ph. 1 calcs: 74 | | | | • | | |

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 24

To Village Ph1 Pond 1

| Hydrograph type | = SCS Runoff | Peak discharge | = 5.507 cfs |
|-----------------|--------------|--------------------|---------------|
| Storm frequency | = 1 yrs | Time to peak | = 722 min |
| Time interval | = 2 min | Hyd. volume | = 15,818 cuft |
| Drainage area | = 8.200 ac | Curve number | = 75 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 10.60 min |
| Total precip. | = 2.26 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 24

To Village Ph1 Pond 1

| Hydrograph type | = SCS Runoff | Peak discharge | = 20.07 cfs |
|-----------------|--------------|--------------------|---------------|
| Storm frequency | = 10 yrs | Time to peak | = 722 min |
| Time interval | = 2 min | Hyd. volume | = 52,546 cuft |
| Drainage area | = 8.200 ac | Curve number | = 75 |
| Basin Slope | = 0.0 % | Hydraulic length | = 0 ft |
| Tc method | = User | Time of conc. (Tc) | = 10.60 min |
| Total precip. | = 4.06 in | Distribution | = Type II |
| Storm duration | = 24 hrs | Shape factor | = 484 |



Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Pond No. 7 - Ex. Village Ph.1 Pond 1

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 2020.00 ft

Stage / Storage Table

| Stage (ft) | Elevation (ft) | Contour area (sqft) | Incr. Storage (cuft) | Total storage (cuft) |
|------------|----------------|---------------------|----------------------|----------------------|
| 0.00 | 2020.00 | 8,930 | 0 | 0 |
| 2.00 | 2022.00 | 11,435 | 20,311 | 20,311 |
| 4.00 | 2024.00 | 14,161 | 25,545 | 45,856 |
| 6.00 | 2026.00 | 17,119 | 31,230 | 77,086 |
| 6.40 | 2026.40 | 17,672 | 6,957 | 84,044 |

Culvert / Orifice Structures

Weir Structures

| | [A] | [B] | [C] | [PrfRsr] | | [A] | [B] | [C] | [D] |
|-----------------|-----------|---------|------|----------|----------------|-------------|-----------|------|------|
| Rise (in) | = 15.00 | 8.00 | 0.00 | 0.00 | Crest Len (ft) | = 3.50 | 20.00 | 0.00 | 0.00 |
| Span (in) | = 15.00 | 8.00 | 0.00 | 0.00 | Crest El. (ft) | = 2024.50 | 2025.50 | 0.00 | 0.00 |
| No. Barrels | = 1 | 1 | 0 | 0 | Weir Coeff. | = 0.90 | 2.50 | 3.33 | 3.33 |
| Invert El. (ft) | = 2020.00 | 2021.00 | 0.00 | 0.00 | Weir Type | = 1 | Broad | | |
| Length (ft) | = 60.00 | 0.00 | 0.00 | 0.00 | Multi-Stage | = Yes | No | No | No |
| Slope (%) | = 1.00 | 0.00 | 0.00 | n/a | | | | | |
| N-Value | = .012 | .012 | .013 | n/a | | | | | |
| Orifice Coeff. | = 0.60 | 0.55 | 0.60 | 0.60 | Exfil.(in/hr) | = 0.000 (by | Wet area) | | |
| Multi-Stage | = n/a | Yes | No | No | TW Elev. (ft) | = 0.00 | | | |

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

| Stage / | Storage / I | Discharge 1 | Fable | | | | . , | | | | | , | |
|-------------|-----------------|-----------------|--------------|--------------|--------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
| 0.00 | 0 | 2020.00 | 0.00 | 0.00 | | | 0.00 | 0.00 | | | | | 0.000 |
| 0.20 | 2,031 | 2020.20 | 0.00 | 0.00 | | | 0.00 | 0.00 | | | | | 0.000 |
| 0.40 | 4,062 | 2020.40 | 0.00 | 0.00 | | | 0.00 | 0.00 | | | | | 0.000 |
| 0.60 | 6,093 | 2020.60 | 0.00 | 0.00 | | | 0.00 | 0.00 | | | | | 0.000 |
| 0.80 | 8,125 | 2020.80 | 0.00 | 0.00 | | | 0.00 | 0.00 | | | | | 0.000 |
| 1.00 | 10,156 | 2021.00 | 0.00 | 0.00 | | | 0.00 | 0.00 | | | | | 0.000 |
| 1.20 | 12,187 | 2021.20 | 0.13 ic | 0.12 ic | | | 0.00 | 0.00 | | | | | 0.124 |
| 1.40 | 14,218 | 2021.40 | 0.43 ic | 0.43 ic | | | 0.00 | 0.00 | | | | | 0.433 |
| 1.60 | 16,249 | 2021.60 | 0.80 ic | 0.80 ic | | | 0.00 | 0.00 | | | | | 0.800 |
| 1.80 | 18,280 | 2021.80 | 1.05 ic | 1.05 ic | | | 0.00 | 0.00 | | | | | 1.052 |
| 2.00 | 20,311 | 2022.00 | 1.29 ic | 1.26 ic | | | 0.00 | 0.00 | | | | | 1.258 |
| 2.20 | 22,866 | 2022.20 | 1.46 ic | 1.43 ic | | | 0.00 | 0.00 | | | | | 1.434 |
| 2.40 | 25,420 | 2022.40 | 1.59 ic | 1.59 ic | | | 0.00 | 0.00 | | | | | 1.591 |
| 2.60 | 27,975 | 2022.60 | 1.73 ic | 1.73 ic | | | 0.00 | 0.00 | | | | | 1.734 |
| 2.80 | 30,529 | 2022.80 | 1.87 ic | 1.87 ic | | | 0.00 | 0.00 | | | | | 1.866 |
| 3.00 | 33,084 | 2023.00 | 2.02 ic | 1.99 ic | | | 0.00 | 0.00 | | | | | 1.989 |
| 3.20 | 35,638 | 2023.20 | 2.11 ic | 2.10 ic | | | 0.00 | 0.00 | | | | | 2.105 |
| 3.40 | 38,193 | 2023.40 | 2.21 ic | 2.21 ic | | | 0.00 | 0.00 | | | | | 2.214 |
| 3.60 | 40,747 | 2023.60 | 2.32 ic | 2.32 ic | | | 0.00 | 0.00 | | | | | 2.319 |
| 3.80 | 43,302 | 2023.80 | 2.42 ic | 2.42 ic | | | 0.00 | 0.00 | | | | | 2.419 |
| 4.00 | 45,856 | 2024.00 | 2.52 ic | 2.52 ic | | | 0.00 | 0.00 | | | | | 2.516 |
| 4.20 | 48,979 | 2024.20 | 2.61 ic | 2.61 ic | | | 0.00 | 0.00 | | | | | 2.608 |
| 4.40 | 52,102 | 2024.40 | 2.70 ic | 2.70 ic | | | 0.00 | 0.00 | | | | | 2.698 |
| 4 60 | 55 225 | 2024 60 | 2 90 ic | 2 78 ic | | | 0.10 | 0.00 | | | | | 2 884 |
| 4 80 | 58 348 | 2024 80 | 3 40 ic | 2 87 ic | | | 0.52 | 0.00 | | | | | 3 385 |
| 5.00 | 61 471 | 2025.00 | 4 07 ic | 2 95 ic | | | 1 11 | 0.00 | | | | | 4 063 |
| 5.20 | 64 594 | 2025 20 | 4 87 oc | 3 03 ic | | | 1 84 | 0.00 | | | | | 4 873 |
| 5 40 | 67 717 | 2025 40 | 5 71 ic | 3 02 ic | | | 2 69 | 0.00 | | | | | 5 707 |
| 5.60 | 70 840 | 2025.60 | 6 61 ic | 2.97 ic | | | 3.63 | 1.57 | | | | | 8 177 |
| 5.80 | 73,963 | 2025.80 | 7.56 ic | 2.90 ic | | | 4 67 | 8 20 | | | | | 15 76 |
| 6.00 | 77 086 | 2026.00 | 8 57 ic | 2 79 ic | | | 5 79 | 17.68 | | | | | 26.25 |
| 6.04 | 77 782 | 2026.00 | 8 78 ic | 2.76 ic | | | 6.02 | 19.84 | | | | | 28.62 |
| 6.08 | 78 478 | 2026.04 | 8 99 ic | 2.70 ic | | | 6.26 | 22.09 | | | | | 31.02 |
| 6.12 | 70,470 | 2026.00 | 9 20 ic | 2.70 ic | | | 6.50 | 24.00 | | | | | 33.61 |
| 6.16 | 70,860 | 2020.12 | 9.20 iC | 2.70 ic | | | 6.74 | 24.42 | | | | | 36.23 |
| 6.20 | 80 565 | 2026.10 | 9.38 ic | 2.67 ic | | | 5.37 ic | 29.30 | | | | | 37.35 |
| 6.24 | 81 261 | 2026.20 | 9.36 ic | 2.00 ic | | | 5.43 ic | 20.00 | | | | | 30.00 |
| 6.24 | 81 957 | 2020.24 | 9.30 ic | 2.7 1 ic | | | 5.40 ic | 34.46 | | | | | 42.60 |
| 0.20 | 01,007 | 2020.20 | 0.0410 | 2.1 + 10 | | 131 | 0.4010 | 57.70 | | | Continue | es on nex | t page |

Ex. Village Ph.1 Pond 1 Stage / Storage / Discharge Table

| Stage ft | Storage cuft | Elevation ft | Clv A cfs | Clv B cfs | Clv C cfs | PrfRsr cfs | Wr A cfs | Wr B cfs | Wr C cfs | Wr D cfs | Exfil cfs | User cfs | Total cfs |
|-------------|-----------------|-----------------|--------------|--------------|--------------|---------------|-------------|-------------|-------------|-------------|--------------|-------------|--------------|
| 6.32 | 82,652 | 2026.32 | 9.32 ic | 2.76 ic | | | 5.55 ic | 37.15 | | | | | 45.46 |
| 6.36 | 83,348 | 2026.36 | 9.30 ic | 2.78 ic | | | 5.61 ic | 39.90 | | | | | 48.30 |
| 6.40 | 84,044 | 2026.40 | 9.28 ic | 2.80 ic | | | 5.67 ic | 42.69 | | | | | 51.17 |

...End

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 25

Village Ph1 Pond 1 Out

| Hydrograph type | = Reservoir | Peak discharge | = 0.132 cfs |
|-----------------|------------------------------|----------------|---------------|
| Storm frequency | = 1 yrs | Time to peak | = 1204 min |
| Time interval | = 2 min | Hyd. volume | = 5,646 cuft |
| Inflow hyd. No. | = 24 - To Village Ph1 Pond 1 | Max. Elevation | = 2021.21 ft |
| Reservoir name | = Ex. Village Ph.1 Pond 1 | Max. Storage | = 12,245 cuft |

Storage Indication method used.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Friday, 04 / 29 / 2022

Hyd. No. 25

Village Ph1 Pond 1 Out

| Hydrograph type | = Reservoir | Peak discharge | = 1.628 cfs |
|-----------------|------------------------------|----------------|---------------|
| Storm frequency | = 10 yrs | Time to peak | = 778 min |
| Time interval | = 2 min | Hyd. volume | = 42,374 cuft |
| Inflow hyd. No. | = 24 - To Village Ph1 Pond 1 | Max. Elevation | = 2022.45 ft |
| Reservoir name | = Ex. Village Ph.1 Pond 1 | Max. Storage | = 26,076 cuft |

Storage Indication method used.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Tuesday, 11 / 1 / 2022

Hyd. No. 32

TOTAL AT PROP LINE PRE

| Hydrograph type Storm frequency | = Combine = 1 vrs | Peak discharge Time to peak | = 75.45 cfs = 726 min |
|------------------------------------|----------------------|--------------------------------|--------------------------|
| Time interval | $= 2 \min$ | Hyd. volume | = 422,747 cuft |
| Inflow hyds. | = 25, 27, 31 | Contrib. drain. area | = 18.140 ac |



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2022

Hyd. No. 32

TOTAL AT PROP LINE PRE

| 4,986 cuft 40 ac |
|---------------------|
| 2 |

